# PASSIVE CONTROL OF MAGNETO-NANOMATERIALS TRANSIENT FLOW SUBJECT TO NON-LINEAR THERMAL RADIATION

by

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Present investigation is concerned with mixed convection flow of Williamson nanoliquid over an unsteady slandering stretching sheet. Aspects of non-linear thermal radiation, Brownian diffusion, and thermophoresis effects are addressed. Non-linear stretching surface of varying thickness induce the flow. Novel features of combined zero mass flux and convective conditions are accounted. Use of appropriate transformations results into the non-linear ODE. Computations for the convergent solutions are provided. Graphs are designed for interpretations to quantities. Nusselt number and surface drag are computationally inspected. Our computed results indicate that attributes of nanoparticles and non-linear thermal radiation enhance the temperature distribution.

Key words: natural and force convection, zero mass flux condition, nanoparticles, non-linear thermal radiation

#### Introduction

Nanomaterials are developed by utilization of tiny less nanometer particles into traditional liquids like water, ethylene glycol and oils. Choi and Eastman [1] firstly illustrated this novel kind of materials known as nanomaterials. These nanometers particles have remarkable physical and chemical characteristics. Such characteristics has motivated several researchers [2-6] to explore the aspects of heat transportation via nanomaterials. They noticed that occurrence of nanoparticles in liquids upsurges crucially the liquid thermal conductance and subsequently ameliorate heat transport properties. Besides this, numerous researchers have recently investigated different convective flow problems regarding nanomaterials, [7, 8]. Buongiorno [2] and Tiwari and Das [3] presented a detailed review regarding convective heat

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transport in nanoliquids. Buongiorno [2] perceived that absolute velocity of nanoparticles can be considered as the addition of base liquid and relative velocities. However, the model given by Tiwari and Das [3] explores response of nanoliquids taking into interpretation the solid volume fraction of nanoliquid. Here we analyze the flow and heat transport features for targeted problem utilizing the model given by Buongiorno [2]. Recently this model has been utilized by several researchers considering different flow situations [9-14].

Solar radiation is the non-polluting and non-conventional inception of energy. Actually this is obtained from radiant light and sun. Recent technology and modern science are greatly compelled towards solar radiation due to its extensive utilizations in photovoltaic cells, solar heating, artificial photosynthesis, solar electricity, *etc.* The small size of nanoparticles in nanomaterials consumes radiation extensively with that of de Broglie wavelength. Thus nanoparticles also declare the favorable quality of ameliorating radiative characteristics of liquids [15]. Few attempts regarding solar radiation can be consulted through [16-18] and several attempts therein. On the other hand the simultaneous natural/forced convective flow (mixed convection flow) has been reported experimentally, analytically and numerically [19-22]. This sort of flow is especially appealing owing to its importance in numerous engineering and industrial utilizations like electronic cooling, chemical process, solar systems, liquid storage tanks, nuclear power technology, *etc*.

Considerable research have been carried out by the researchers for the analysis of laminar flow by moving surface owing to its ever growing industrial utilizations in condensation process, glass and polymer industries, cooling procedure of metallic plate in cooling bath, and plastic sheets discharge. Sakiadis [23] led the basis for the stretched flow problem. Extensive analyses covering numerical and analytical investigations interpreting diverse characteristics of stretched flow are made [24-26]. Surface with varying thickness finds demand in nuclear reactor technology, acoustical components, machine design, architecture, naval structures, *etc.* The idea of varying thickness sheet initiated all the way through linearly deforming materials like nozzles and needles. Lee [27] initiated the idea of varying thickness. Afterwards other researchers [28-31] considered flow features by slendering sheet.

The novelty of current article is to explore the aspects of non-linear thermal radiation and mixed convection in unsteady flow of Williamson nanofluid bounded by unsteady slendering sheet. Energy and concentration expressions are characterized through Brownian motion and thermophoresis phenomena. Implementation of homotopic scheme [32-34] help us to analyze governing mathematical problems. Plots have been interpreted to examine the characteristics of key variables. Representation of skin friction and Nusselt number have been numerically examined.

#### **Problems development**

Here mathematical formulation for unsteady mixed convection 2-D flow of Williamson liquid stretching sheet of variable thickness,  $y = \delta(x + b)^{(1-n)/2}$ ,  $\delta$  being small, is given. Let  $u = U_0[(x+b)^n/(1-\gamma_1 t)]$  declares the sheet velocity, fig. 1. Further keep in mind that n = 1 corresponds to flat stretching surface. Buoyancy force effects are considered. Energy expression is radiation and convective surface condition. Novel aspects of zero mass flux condition is also taken at the surface. The aspects of thermophoretic and Brownian diffusions are accounted. Ambient and sheet fluid concentrations and temperatures are symbolized by  $(C_w, T_f)$  and  $(C_\infty, T_\infty)$  respectively. The resulting boundary layer problems are defined by [10, 35-37]:



Figure 1. Flow geometry

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = v \frac{\partial^2 u}{\partial y^2} + 2v \Gamma \frac{\partial u}{\partial y} \left( \frac{\partial^2 u}{\partial y^2} \right) + g \beta_{\Gamma} (T - T_{\infty}) + g \beta_{C} (C - C_{\infty})$$
(2)

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha_m \frac{\partial^2 T}{\partial y} + \frac{(\rho c)_p}{(\rho c)_f} \left[ D_B \frac{\partial T}{\partial y} \frac{\partial C}{\partial y} + \frac{D_T}{T_{\infty}} \left( \frac{\partial T}{\partial y} \right)^2 \right] - \frac{1}{(\rho c)_f} \frac{\partial q_r}{\partial y}$$
(3)

$$\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = \left(\frac{D_{\rm T}}{T_{\infty}}\right) \frac{\partial^2 T}{\partial y^2} + D_B \frac{\partial^2 C}{\partial y^2} \tag{4}$$

with

$$u = U_w(x,t) = \frac{(x+b)^n}{(1-\gamma_1 t)} U_0, \quad v(x,t) = 0, \quad -k\frac{\partial T}{\partial y} = h_f(T_f - T)$$

$$D_B \frac{\partial C}{\partial y} + \frac{D_T}{T_\infty} \frac{\partial T}{\partial y} = 0 \text{ at } y = \delta(x+b)^{\frac{1-n}{2}}$$

$$u \to 0, \quad T \to T_\infty, \quad C \to C_\infty \text{ as } y \to \infty$$
(6)

where (u, v) denotes the liquid velocities in direction of x- and y-axis, b and  $\gamma_1$  – the rate constants with b > 0 and  $\gamma_1 \ge 0$ ,  $\Gamma$  – the time constant, g – the gravitational acceleration,  $\mu_0$  –

the dynamic viscosity,  $h_f$  – the coefficient of heat transport,  $\rho_f$  – the density of liquid,  $\beta_T$  and  $\beta_C$  – the coefficient of (thermal, solutal) expansions, T and  $T_0$  stand for liquid and reference temperatures, n – the velocity power index,  $(\rho c)_f$ ,  $(\rho c)_p$  – the liquid and nanoparticles capacities,  $q_r$  – the radiative heat flux,  $D_B$  – the diffusion coefficient,  $C_0$ , and C – the reference and fluid concentrations,  $\nu$  – the kinematic viscosity,  $\alpha_m = k/(\rho c)_f$  for the thermal diffusivity, and  $D_T$  – the coefficient of thermophoretic diffusion.

The radiative heat flux  $q_r$  estimation is:

$$q_{\rm r} = -\frac{4\sigma^{**}}{3m^{**}}\frac{\partial(T^4)}{\partial y} = -\frac{16\sigma^{**}T^3}{3m^{**}}\frac{\partial T}{\partial y}$$
(7)

where  $\sigma^{**}$  designates the Stefan-Boltzman and  $m^{**}$  symbolized the coefficient of mean absorption. Upon using eq. (7), the energy expression becomes:

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \alpha_m \frac{\partial^2 T}{\partial y^2} + \frac{(\rho c)_p}{(\rho c)_f} \left[ D_B \frac{\partial T}{\partial y} \frac{\partial C}{\partial y} + \frac{D_T}{T_{\infty}} \left( \frac{\partial T}{\partial y} \right)^2 \right] - \frac{1}{(\rho c_p)} \frac{\partial}{\partial y} \left( \frac{16\sigma^{**}T^3}{3m^{**}} \frac{\partial T}{\partial y} \right)$$
(8)

By invoking the following transformations:

$$u = U_0 \frac{(x+b)^n}{1-\gamma_1 t} F'(\eta), \quad v = -\sqrt{\frac{n+1}{2}} v U_0 \frac{(x+b)^{n-1}}{1-\gamma_1 t} \left[ F(\eta) + \eta F'(\eta) \frac{n-1}{n+1} \right]$$

$$\eta = y \sqrt{\frac{n+1}{2}} \frac{U_0 (x+b)^{n-1}}{v(1-\gamma_1 t)}, \quad \Theta(\eta) = \frac{T-T_\infty}{T_f - T_\infty}, \quad \Phi(\eta) = \frac{C-C_\infty}{C_\infty}$$
(9)

Equation (1) reduces trivially while other eqs. (2)-(6) and (8) are:

$$F''' + FF'' - \left(\frac{2n}{n+1}\right)F'^2 - \left(\frac{n}{n+1}\right)\left(\frac{\eta}{2}F'' + F'\right) + \sqrt{\frac{n+1}{2}}\operatorname{We}F''F''' + \lambda(\Theta + N\Phi) = 0 \quad (10)$$

$$\left(1 + \frac{4}{3}Rd\right) + \frac{4}{3}Rd[(\theta_w - 1)^3(3\Theta'^2\Theta'^2 + \Theta^3\Theta'') + 3(\theta_w - 1)^2(2\Theta'^2\Theta + \Theta^2\Theta'') + 3(\theta_w - 1)(\Theta'^2 + \Theta\Theta'')] - (10)$$

$$-\Pr\left[A\frac{n}{n+1}(\Theta+\eta\Theta') + \frac{1-n}{1+n}F'\Theta - F\Theta' - N_{b}\Theta'\Phi' - N_{t}\Theta'^{2}\right] = 0$$
(11)

$$\Phi'' + \operatorname{Sc}\left[A\frac{n}{n+1}(\Phi + \eta\Phi') + \left(\frac{1-n}{1+n}\right)F'\Phi - F\Phi'\right] + \left(\frac{N_{\mathrm{t}}}{N_{\mathrm{b}}}\right)\Theta'' = 0$$
(12)

$$F(\alpha) = \alpha \frac{1-n}{1+n}, \quad F'(\alpha) = 1, \quad F'(\infty) \to 0$$
  
$$\Theta'(\alpha) = -\gamma [1 - \Theta(\alpha)], \quad \Phi'(\alpha) + \frac{N_{\rm t}}{N_{\rm b}} \Theta'(\alpha) = 0 \tag{13}$$
  
$$\Theta(\infty) \to 0, \quad \Phi(\infty) \to 0$$

where

$$\alpha = \delta \sqrt{\frac{n+1}{2} \frac{U_0}{v}}$$

designates wall thickness parameter and:

$$\alpha = \eta = \delta \sqrt{\frac{n+1}{2} \frac{U_0}{v}}$$

Considering

$$F(\eta) = f(\eta - \alpha) = f(\xi), \quad \Theta(\eta) = \theta(\eta - \alpha) = \theta(\xi), \quad \Phi(\eta) = \phi(\eta - \alpha) = \phi(\xi)$$
(14)

Equation (8) and eqs. (10)-(13) yield:

$$f''' + ff'' - \left(\frac{2n}{n+1}\right)f'^2 - \left(\frac{n}{n+1}\right)\left(\frac{\xi}{2}f'' + f'\right) + \sqrt{\frac{n+1}{2}}\operatorname{Wef}''f''' + \lambda(\theta + N\phi) = 0$$
(15)

$$\left(1 + \frac{4}{3}Rd\right) + \frac{4}{3}Rd[(\theta_w - 1)^3(3\theta'^2\theta^2 + \theta^3\theta'') + 3(\theta_w - 1)^2(2\theta'^2\theta + \theta^2\theta'') + 3(\theta_w - 1)(\theta'^2 + \theta\theta'')] - 1$$

$$-\Pr\left[A\frac{n}{1+n}(\theta+\xi\theta')+\frac{1-n}{1+n}f'\theta-f\theta'-N_{\rm b}\theta'\phi'-N_{\rm t}\theta'^2\right]=0$$
(16)

$$\phi'' + \operatorname{Sc}\left[A\frac{n}{n+1}(\phi + \xi\phi') + \frac{1-n}{1+n}f'\phi - f\phi'\right] + \frac{N_{\mathrm{t}}}{N_{\mathrm{b}}}\theta'' = 0$$
(17)

$$f(0) = \alpha \frac{1-n}{1+n}, \quad f'(0) = 1, \quad f'(\infty) \to 0$$
  
$$\theta'(0) = -\gamma [1-\theta(0)], \quad \phi'(0) + \frac{N_{\rm t}}{N_{\rm b}} \theta'(0) = 0 \tag{18}$$
  
$$\theta(\infty) \to 0, \quad \phi(\infty) \to 0$$

where  $\lambda$  is the mixed convection variable, Pr – the Prandtl number, N – the buoyancy ratio,  $N_t$  – the thermophoresis variable,  $N_b$  – the Brownian motion variable, Sc – the Schmidt number, We – the Weissenberg number,  $\theta_w$  – the temperature ratio parameter, A – the unsteadiness parameter,  $\gamma$  – the convective parameter, Re<sub>x</sub> – the Reynolds number, and Rd – the radiation variable. These variables are:

$$A = \frac{\gamma_{1}(b+x)^{1-n}}{U_{0}}, \quad \lambda = \frac{\mathrm{Gr}_{x}}{\mathrm{Re}_{x}^{2}}, \quad \mathrm{Gr}_{x} = \frac{\mathrm{g}\beta_{\mathrm{T}}(T_{f} - T_{\infty})(b+x)^{3}}{v^{2}}, \quad \gamma = \frac{h_{f}}{k} \sqrt{\frac{2\nu(b+x)}{(n+1)U_{w}}}$$

$$N = \frac{\beta_{C}C}{\beta_{\mathrm{T}}(T_{f} - T_{\infty})}, \quad \mathrm{Pr} = \frac{\nu}{\alpha_{m}}, \quad \mathrm{Sc} = \frac{\nu}{D_{B}}, \quad N_{b} = \frac{(\rho c)_{p}}{(\rho c)_{f}} \frac{D_{B}C_{\infty}}{v}$$

$$N_{t} = \frac{(\rho c)_{p}}{(\rho c)_{f}} \frac{D_{\mathrm{T}}(T_{f} - T_{\infty})}{T_{\infty}v}, \quad Rd = \frac{4\sigma^{**}T_{\infty}^{3}}{m^{**}k}, \quad \mathrm{We} = \Gamma \frac{\sqrt{U_{0}^{3}(b+x)^{3n-1}}}{(1-\gamma_{1}t)^{3}}, \quad \mathrm{Re}_{x} = U_{w} \frac{b+x}{v}$$

$$(19)$$

The expressions of skin friction,  $C_{f_x}$ , and local heat flux rate at the surface, Nu<sub>x</sub>, are:

$$C_{f_{x}} = \frac{\tau_{yx}|_{y=\delta(b+x)^{\frac{1-n}{2}}}}{\frac{1}{2}\rho U_{w}^{2}} \models \frac{\mu_{0} \left[\frac{\partial u}{\partial y} + \frac{\Gamma}{2} \left(\frac{\partial u}{\partial y}\right)^{2}\right]_{y=\delta(b+x)^{\frac{1-n}{2}}}}{\rho U_{w}^{2}}$$
(20)

$$Nu_{x} = (q_{r})_{w} + \frac{(b+x)q_{w}|_{y=\delta(b+x)^{\frac{b-a}{2}}}}{D_{B}(T_{f}-T_{\infty})} = -\frac{\left(\frac{\partial T}{\partial y}\right)_{y=\delta(b+x)^{\frac{b-a}{2}}}}{T_{f}-T_{\infty}} + (q_{r})_{w}$$
(21)

In non-dimensional form we have:

$$(\operatorname{Re}_{x})^{0.5}C_{f_{x}} = \sqrt{\frac{(n+1)}{2}}f''(0) + \frac{(n+1)}{4}\operatorname{We}f^{''2}(0)$$
(22)

$$(\operatorname{Re}_{x})^{-0.5}\operatorname{Nu}_{x} = \sqrt{\left(\frac{n+1}{2}\right)} \left(1 + \frac{4}{3}Rd\left\{1 + (\theta_{w} - 1)[\theta(0)]^{3}\right\}\right)\theta'(0)$$
(23)

## Analysis of convergent solutions

We select initial guesses  $(f_0, \theta_0, \phi_0)$  and linear operators  $((\mathbf{\bar{L}}_f, \mathbf{\bar{L}}_\theta, \mathbf{\bar{L}}_\phi))$  in the forms:

$$f_0(\xi) = \alpha \frac{1-n}{1+n} + 1 - e^{-\xi}$$
  

$$\theta_0(\xi) = \frac{\gamma}{1+\gamma} e^{-\xi}$$
  

$$\phi_0(\xi) = -\frac{\gamma}{1+\gamma} \frac{N_t}{N_b} e^{-\xi}$$
(24)

with

$$\overline{\mathbf{L}}_{f} \left[ D_{1}^{**} + D_{2}^{**} e^{\xi} + D_{3}^{**} e^{-\xi} \right] = 0$$

$$\overline{\mathbf{L}}_{\theta} \left[ D_{4}^{**} e^{\xi} + D_{5}^{**} e^{-\xi} \right] = 0$$

$$\overline{\mathbf{L}}_{\phi} \left[ D_{6}^{**} e^{\xi} + D_{7}^{**} e^{-\xi} \right] = 0$$
(25)

where  $D_i^{**}$  (*i* = 1-7) declared arbitrary constants and have the following values:

$$D_{2}^{**} = D_{4}^{**} = D_{6}^{**} = 0, \quad D_{3}^{**} = \frac{\partial f_{m}^{*}(\xi)}{\partial \xi}|_{\xi=0}, \quad D_{1}^{**} = -D_{3}^{**} - f_{m}^{*}(0)$$

$$D_{5}^{**} = \frac{1}{1+\gamma} \frac{\partial \theta_{m}^{*}(\xi)}{\partial \xi}|_{\xi=0} - \frac{\gamma}{1+\gamma} \theta_{m}^{*}(0), \quad D_{7}^{**} = \frac{\partial \phi_{m}^{*}(\xi)}{\partial \xi}|_{\xi=0} + \frac{N_{t}}{N_{b}} \left[ \frac{\partial \theta_{m}^{*}(\xi)}{\partial \xi}|_{\xi=0} \theta_{m}^{*}(0) \right]$$
(26)

Homotopic scheme secure us regarding the convergence of approximate solutions. Here embedding variables  $\hbar_f$ ,  $\hbar_{\theta}$ , and  $\hbar_{\phi}$  have key role in convergence of derived solutions. Figures 2 and 3 indicated the  $\hbar$ -curves which enable us to pointed out the estimations for  $\hbar_f$ ,  $\hbar_{\theta}$ , and  $\hbar_{\phi}$ . These acceptable ranges are ( $-0.5 \le \hbar_f \le -1.5$ ), ( $-0.50 \le \hbar_{\theta} \le -1.84$ ), and ( $-0.20 \le \hbar_{\phi} \le -1.86$ ). Moreover the convergence of HAM is inspected through tab. 1. It is noticed from tab.1 that series solutions converge up to 35<sup>th</sup> order of estimations for velocity whereas 40<sup>th</sup> order of deformations are ample for the temperature and concentration distributions.





Figure 2. The  $\hbar$  -curve for *f*;  $\alpha = 0.3$ , We = *N* = = *Rd* = 0.2 =  $\gamma$  = *Nt*, *Nb* = 0.5, Pr = 0.8 = Sc, *A* = 1.0,  $\lambda$  = 0.1, *n* = 0.9

Figure 3. The  $\hbar$  -curve for  $\theta(\zeta)$  and  $\phi(\zeta)$ ;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma = Nt$ , Nb = 0.5, Pr = 0.8 = Sc,  $A = 1.0, \lambda = 0.1, n = 0.9$ 

Table 1. Convergence when  $Rd = N = 0.2 = We = \gamma = N_t$ ,  $\alpha = 0.3$ ,  $A = 1.0 = \theta_w$ ,  $\lambda = 0.1$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc, and n = 0.9

Order of estimations	-f''(0)	- heta'(0)	φ'(0)
1	1.05802	0.15715	0.06286
10	1.14303	0.12665	0.05065
15	1.14399	0.12421	0.04968
20	1.14402	0.12419	0.04968
35	1.14403	0.12413	0.04958
40	1.14403	0.12412	0.04951
45	1.14403	0.12412	0.04951
50	1.14403	0.12412	0.04951
55	1.14403	0.12412	0.04951

## Discussion

Features of various involved variables on  $f(\zeta)$ ,  $\theta(\zeta)$ ,  $\phi(\zeta)$ ,  $-(\text{Re})^{1/2}C_{f_{\chi}}$ , and Nu<sub>x</sub> are investigated in this section. Such goal is achieved *via* figs. 4-21 and tabs. 2 and 3. Aspects of  $\alpha$  on  $f(\zeta)$  is depicted in fig. 4. Here decay in  $f(\zeta)$  is remarked against  $\alpha$ . Features of  $f(\zeta)$  due to higher *n* is designed in fig. 5. Here velocity grows in response of higher *n*. Increase in *n* improves the surface velocity, which speed up liquid deformation. Behavior of  $f(\zeta)$  vs.  $\lambda$  is interpreted in fig. 6. Clearly velocity rises *via*  $\lambda$ . Physically larger  $\lambda$  accompany a stronger buoyancy force and it leads to an increment in  $f(\zeta)$ . Velocity  $f(\zeta)$  against *N* is exhibited in fig. 7.



Figure 3. Response of  $f'(\zeta)$  against  $\alpha$ ; We = N = =  $Rd = 0.2 = \gamma = N_{\rm t}, \ \theta_w = 1.2, \ N_{\rm b} = 0.5, \ Pr = 0.8 = Sc, \ A = 1.0, \ \lambda = 0.1, \ n = 0.9$ 



Figure 5. Response of  $f'(\xi)$  against  $\lambda$ ;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = = 0.8 = Sc, A = 1.0, n = 0.9



Figure 7. Response of  $f'(\zeta)$  against *A*;  $\alpha = 0.3$ , We = *N* = *Rd* = 0.2 =  $\gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc,  $\lambda = 0.1$ , *n* = 0.9



Figure 4. Response of  $f'(\xi)$  against *n*;  $\alpha = 0.3$ , We = *N* = *Rd* = 0.2 =  $\gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc, *A* = 1.0,  $\lambda = 0.1$ 



Figure 6. Response of  $f'(\xi)$  against N;  $\alpha = 0.3$ , We = 1.2,  $Rd = 0.2 = \gamma = N_t$ ,  $\theta_w = N_b = 0.5$ , Pr = 0.8 = Sc, A = 1.0,  $\lambda = 0.1$ , n = 0.9



Figure 8. Response of  $f'(\xi)$  against We;  $\alpha = 0.3$ ,  $N = Rd = 0.2 = \gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc, A = 1.0,  $\lambda = 0.1$ , n = 0.9

Here  $f(\zeta)$  grow up against *N*. Consequences of *A* on  $f(\zeta)$  is depicted in fig. 8. For higher *A* the rate of stretching is smaller in *x*-direction which eventually diminish  $f(\zeta)$ . Effect of We on  $f(\zeta)$  is shown in fig. 9. Larger We decays  $f(\zeta)$ . Aspects of  $\alpha$  on  $\theta(\zeta)$  is presented in fig. 10. Here temperature field decays when  $\alpha$  is enhanced. Variation of  $\theta(\zeta)$  via *n* is designated in





Figure 9. Response of  $\theta(\xi)$  against  $\alpha$ ; We = N = Rd = 0.2 =  $\gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc, A = 1.0,  $\lambda = 0.1$ , n = 0.9

Figure 10. Response of  $\theta(\xi)$  against *n*;  $\alpha = 0.3$ , We = *N* = *Rd* = 0.2 =  $\gamma = N_{\rm t}$ ,  $\theta_{\rm w} = 1.2$ ,  $N_{\rm b} = 0.5$ , Pr = 0.8 = Sc, *A* = 1.0,  $\lambda = 0.1$ 

fig. 11. Here temperature field enhances for larger n. Higher temperature  $\theta(\zeta)$  is liked with higher  $\lambda$ , fig. 12. In fact, higher  $\lambda$  leads to higher buoyancy forces which results in an increment of  $\theta(\xi)$ . Impact of N on  $\theta(\xi)$  is explored through fig. 13. Here temperature is decreasing function of N. Physically N is the ratio of concentration to thermal buoyancy forces. Thus an enhancement in N corresponds to lower temperature. Remarkable features of  $\theta(\xi)$  against N<sub>t</sub> is displayed in fig. 14. It is inspected that  $\theta(\zeta)$  is boosted via  $N_t$ . It is because of the fact that in thermophoresis process, the heated liquid particles extracted towards cold regime from hot surface which corresponds to boosts up  $\theta(\zeta)$ . Through fig. 15 the characteristics of Pr on temperature distribution is reported. For larger Pr the fluid temperature reduces. It is due to low rate of thermal diffusion which associates to larger Pr. It leads to reduction temperature. Figure 16 indicates influence of Rd on  $\theta(\zeta)$ . It is noted that  $\theta(\zeta)$  increases when Rd enhances. It is important to remark that in radiation process, extra heat is added nanomaterials and thus temperature rises. Role of  $\gamma$  on  $\theta(\xi)$  is pointed out in fig. 17. Here  $\theta(\xi)$  rises for  $\gamma$  fig. 18 is displayed to examine the variation of  $N_t$  on  $\phi(\zeta)$ . It is disclosed that  $\phi(\zeta)$  is lower for  $N_t$ . Effect of  $N_{\rm b}$  on  $\phi(\xi)$  is explored in fig. 19. Here  $\phi(\xi)$  diminishes for  $N_{\rm t}$ . The curves of concentration  $\phi(\zeta)$  for Sc are declared in fig. 20. Here it is inspected that grows in Sc decays concentration. Concentration is reduced via *n*, fig. 21. Numerical investigation of  $-(\text{Re})1/2C_{f_x}$  for involved variables of interest is executed in tab. 2. Here we pointed out that for increasing  $\theta_{w}$ , n, A, and  $\alpha$ , the skin friction is increased. Table 3 is prepared to explain features of quantities on Nu<sub>x</sub>. It is noticed that Nu<sub>x</sub> enhances for N, Rd,  $\gamma$ , N<sub>b</sub>, N<sub>b</sub>, and  $\theta_w$ .



Figure 11. Response of  $\theta(\zeta)$  against  $\lambda$ ;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma = N_{\rm t}$ ,  $\theta_{\rm w} = 1.2$ ,  $N_{\rm b} = 0.5$ , Pr =  $0.8 = {\rm Sc}$ , A = 1.0, n = 0.9



Figure 12. Response of  $\theta(\xi)$  against *N*;  $\alpha = 0.3$ , We = *Rd* = 0.2 =  $\gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc, *A* = 1.0,  $\lambda = 0.1$ , *n* = 0.9



Figure 13. Response of  $\theta(\zeta)$  against  $N_t$ ;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma = N_t$ ,  $\theta_w = 1.2$ , Pr = 0.8 = Sc, A = 1.0,  $\lambda = 0.1$ , n = 0.9



Figure 15. Response of  $\theta(\xi)$  against *Rd*;  $\alpha = 0.3$ , We = *N* = 0.2 =  $\gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc, *A* = 1.0,  $\lambda = 0.1$ , *n* = 0.9



Figure 17. Response of  $\phi(\xi)$  against  $N_t$ ;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = = Sc, A = 1.0,  $\lambda = 0.1$ , n = 0.9



Figure 14. Response of  $\theta(\xi)$  against Pr;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Sc = 0.8, A = 1.0,  $\lambda = 0.1$ , n = 0.9



Figure 16. Response of  $\theta(\zeta)$  against  $\gamma$ ;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8 = Sc, A = 1.0,  $\lambda = 0.1$ , n = 0.9



Figure 18. Response of  $\phi$  ( $\xi$ ) against  $N_b$ ;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma = N_t$ ,  $\theta_w = 1.2$ , Pr = 0.8 = Sc, A = 1.0,  $\lambda = 0.1$ , n = 0.9





Figure 19. Response of  $\phi$  ( $\xi$ ) against Sc;  $\alpha = 0.3$ , We =  $N = Rd = 0.2 = \gamma = N_t$ ,  $\theta_w = 1.2$ ,  $N_b = 0.5$ , Pr = 0.8, A = 1.0,  $\lambda = 0.1$ , n = 0.9

Figure 20. Response of  $\phi$  ( $\xi$ ) against *n*;  $\alpha = 0.3$ , We = *N* = *Rd* = 0.2 =  $\gamma = N_{t}$ ,  $\theta_{w} = 1.2$ ,  $N_{b} = 0.5$ , Pr = 0.8 = Sc, *A* = 1.0,  $\lambda = 0.1$ 

Tab	ole 2	. 1	Numerical	simulation	for	surface	drag	force -	-(Re) <sup>0.</sup>	${}^{5}C_{fx}$
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Variable (fixed values)	Parameters		$-({\rm Re})^{1/2}C_{fx}$
		0.5	1.43310
$N = \text{We} = Rd = 0.2 = \gamma = N_{\text{t}} \alpha = 0.3,$ $A = 1.0 = 0.1  N_{\text{t}} = 0.5  \text{Pr} = 0.8 = 52$	x = 0.3, n 1.0 1.78509	1.78509	
$A = 1.0 - 0_{W}, \lambda = 0.1, N_{\rm b} = 0.3, F1 = 0.8 - Sc$		1.5	0.19674
	1, We	0.0	2.21832
$N = Rd = 0.2 = \gamma = N_{\rm t}, \alpha = 0.3, A = 1.0 = \theta_{\rm w}, \lambda = 0.1,$ $N_{\rm t} = 0.5 \text{ Pr} = 0.8 = S_{\rm c}, n = 0.9$		0.2	1.88636
$N_{\rm b} = 0.5,  {\rm Pr} = 0.8 = {\rm Sc},  n = 0.9$		0.4	1.71881
	α	0.0	1.70861
$N = We = Rd = 0.2 = \gamma = N_t, A = 1.0 = \theta_w,$ $\lambda = 0.1, N_t = 0.5, Pr = 0.8 = Sc, n = 0.9$		0.3	1.72056
$\lambda = 0.1, 1 = 0.5, 11 = 0.5 = 50, n = 0.5$		0.6	1.73170
		0.0	1.71622
We = $Rd = 0.2 = \gamma = N_t, \alpha = 0.3,$ $\lambda = 0.1, N_b = 0.5, Pr = 0.8 = Sc, n = 0.9$	Ν	0.3	1.72107
x = 0.1, 100 = 0.0, 11 = 0.0 = 50, n = 0.9		0.7	1.72707
	Α	0.0	1.60630
$N = We = Rd = 0.2 = \gamma = N_t, \alpha = 0.3, \theta_w = 1.0,$ $A = 1.0 - \theta_w, \lambda = 0.1, N_b = 0.5, Pr = 0.8 - Sc, n = 0.9$		0.5	1.70459
$n = 1.0 - 6_{W}, n = 0.1, n_0 = 0.3, 11 - 0.0 - 50, n = 0.9$		1.0	1.72056
	$ heta_w$	0.5	1.23240
$N = \text{We} = Rd = 0.2 = \gamma = N_{\text{t}} \alpha = 0.3, A = 1.0, \lambda = 0.1,$ $N_{\text{b}} = 0.5 \text{ Pr} = 0.8 = \text{Sc} n = 0.9$		1.0	1.24561
$n_0 = 0.3, 11 = 0.0 = 50, n = 0.9$		1.5	1.28657
		0.1	1.71802
$N = \text{We} = Rd = 0.2 = \gamma, \alpha = 0.3, A = 1.0 = \theta_w, \lambda = 0.1,$ Nh = 0.5 Pr = 0.8 = Sc, n = 0.9	$N_{ m t}$	0.3	1.72356
$N_0 = 0.3, 11 = 0.0 = 50, n = 0.9$		0.5	1.73000
	Nb	0.0	1.73435
$N = We = Rd = 0.2 = \gamma = N_t, \alpha = 0.3,$ $A = 1.0 - \theta, \lambda = 0.1 Pr = 0.8 - Sc, n = 0.9$		0.4	1.72138
$n = 1.0 - 0_W, n = 0.1, 11 - 0.0 - 50, n = 0.7$		0.6	1.71939
	γ	0.0	1.75820
$N = We = Kd = 0.2 = N_t, \alpha = 0.3,$ A - 1 0 - $\theta_{w}$ $\lambda = 0.1$ N <sub>b</sub> = 0.5 Pr = 0.8 - Sc $n = 0.9$		0.2	1.72090
$n = 1.0 - 6_{W}, n = 0.1, n_0 = 0.3, 11 - 0.0 - 50, n = 0.7$		0.4	1.70660

1415

## Ullah, I., et al.: Passive Control of Magneto-Nanomaterials Transient Flow Subject ... THERMAL SCIENCE: Year 2022, Vol. 26, No. 2B, pp. 1405-1419

Table 3.	Numerical	data	of Nu <sub>x</sub>
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Variable (fixed values)	Parameters		$-\left(\frac{n+1}{2}\right)^{1/2}\theta'(0)$
$N = We = Rd = 0.2 = N_t \alpha = 0.3$		0.5	0.09808
$A = 1.0 = \theta_w, \lambda = 0.1, N_b = 0.5, Pr = 0.8 = Sc$	п	1.0	0.16103
		1.5	2.06351
		0.0	0.15243
$N = Rd = 0.2 = \gamma = N_t, \alpha = 0.3,$ $A = 1.0 = \theta_{w}, \lambda = 0.1, N_b = 0.5, Pr = 0.8 = Sc, n = 0.9$	We	0.2	0.15327
n = 10 = 00, n = 0.1, 10 = 0.0, 11 = 0.0 = 0.0, n = 0.0		0.4	0.15636
		0.0	0.15247
$N = \text{We} = Rd = 0.2 = \gamma = N_{\text{t}},$ $A = 1.0 = \theta_{\text{w}}, \lambda = 0.1, N_{\text{b}} = 0.5, \text{Pr} = 0.8 = \text{Sc}, n = 0.9$	α	0.3	0.15225
n = 10 = 00, n = 0.1, 10 = 0.0, 11 = 0.0 = 0.0, n = 0.0		0.6	0.15348
		0.0	0.15295
We = $Rd = 0.2 = \gamma = N_t, \alpha = 0.3,$ $A = 1.0 = \theta_{w}, \lambda = 0.1, N_b = 0.5, Pr = 0.8 = Sc, n = 0.9$	Ν	0.3	0.15336
n = 1.0 = 0.0, n = 0.1, 10 = 0.0, 11 = 0.0 = 0.0, n = 0.0		0.7	0.15338
	Α	0.0	0.05466
$N = \text{We} = Rd = 0.2 = \gamma = N_{\text{t}}, \alpha = 0.3, \theta_w = 1.0, \lambda = 0.1,$ $N_{\text{b}} = 0.5 \text{ Pr} = 0.8 = \text{Sc}, n = 0.9$		0.5	0.12733
100 - 0.0, 11 - 0.0 - 0.0, n - 0.0		1.0	0.15225
	$ heta_w$	0.5	0.13423
$N = \text{We} = Rd = 0.2 = \gamma = N_t, \alpha = 0.3,$ $A = 1.0, \lambda = 0.1, N_b = 0.5, \text{Pr} = 0.8 = \text{Sc}, n = 0.9$		1.0	0.17685
$n = no, n = 0.1, n_0 = 0.0, n = 0.0 = 0.0, n = 0.0$		1.5	0.19254
	Nt	0.1	0.15258
$N = We = Rd = 0.2 = \gamma, \alpha = 0.3,$ $A = 1.0 = \theta_{w}, \lambda = 0.1, N_{b} = 0.5, Pr = 0.8 = Sc, n = 0.9$		0.3	0.15238
n = 10 = 00, n = 0.1, 10 = 0.0, 11 = 0.0 = 50, n = 0.5		0.5	0.15222
	$N_{ m b}$	0.0	0.15301
$N = \text{We} = Rd = 0.2 = \gamma = N_t, \alpha = 0.3,$ $A = 1.0 - \theta_{w}, \lambda = 0.1$ Pr = 0.8 - Sc, $n = 0.9$		0.4	0.15225
n = 1.0 - 0 w, $n = 0.1$ , $n = 0.0 - 50$ , $n = 0.7$		0.6	0.15242
	γ	0.0	0.00000
$N = \text{We} = Rd = 0.2 = N_{\text{t}}, \alpha = 0.3,$ $A = 10 - \theta_{\text{tr}}, \lambda = 0.1, N_{\text{b}} = 0.5, \text{Pr} = 0.8 = S_{\text{c}}, n = 0.9$		0.2	0.15211
$n = 1.0 - 6_{W}, n = 0.1, m_0 - 0.5, 11 - 0.0 - 50, n = 0.9$		0.4	0.21916

## Conclusions

In the current study we investigated non-linear thermal radiation in mixed convection flow of Williamson nanoliquid bounded by slendering stretching surface subjected to convective and zero mass flux conditions. The following points are as follows.

- Enhancement in unsteadiness parameter decays velocity.
- Velocity power index exhibits an opposite effect for velocity and temperature fields.
- Higher  $\gamma$ ,  $\lambda$ , and *Rd* rises the temperature.

- Impact of  $N_b$  on  $\phi(\xi)$  is qualitatively revers to that of  $N_t$ .
- Velocity and temperature fields are increasing function of mixed convection parameter  $\lambda$ .
- Skin friction and heat transfer coefficients are enhanced via unsteadiness variable and velocity power index.
- The HAM technique may use for different engineering problems and compared with solution obtained through different techniques [38-45].

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