

DARCY-FORCHHEIMER CHARACTERISTICS OF VISCOELASTIC STRATIFIED NANOLIQUID BY CONVECTIVELY HEATED PERMEABLE SURFACE

by

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A non-linear mathematical analysis for non-Darcian magneto-viscoelastic nanoliquid is elaborated in this research. Flow is caused by stratified surface having permeable nature. The Robin's type boundary conditions are imposed at moving surface. Brownian diffusion, heat source and thermophoretic aspects are accounted. Complex systems are simplified through the well-known boundary-layer concept which is subsequently transfigured to ordinary ones via transformation technique. Furthermore the meaningful physical variables arising in non-dimensional problems are elucidated via graphs.

Key words: *viscoelastic stratified nanoliquid, permeable surface, thermophoresis, Brownian movement, Heat generation,*

Introduction

It is well-known that orthodox heat transferring materials for illustration water, ethylene-glycol (EG) and mineral oil have inadequate heat transport characteristics in comparison solids. An innovative approach regarding liquids heat transport is to adjoin smaller solid elements in liquids. This innovative class of liquid identified as nanoliquid was firstly elaborated by Choi and Eastman [1]. Nanoliquid elaborates a solid-liquid concoction comprising fundamental lower volume fraction having higher conductivity solid nanoparticles. Such liquids have ample uses for instance melt-spinning, production of glass-fiber, airplanes and micro-reactors, *etc.* Researchers considered nanoliquid mechanisms like thermal diffusion, thermophoretic, particle-particle coupling, Brownian movement, micro-convection, and conduction subjected to aggregates. Some experimental researches declare nanoparticles Brownian movement is leading aspect that significantly affect liquids thermal competence. Few recent analyses featuring nanoliquid dynamics under distinct characteristics are mentioned in [2-10].

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Another appealing approach for heat transference improvement in industrial structures is the consideration of porous medium for illustration, the utilization of porous materials based on metal like copper froths in heat exchangers and channel. Indeed porous medium encompasses of miniscule stomas in which liquid-flows. Solar receivers, energy storage units and extraction/percolation of oil through wells are prospective utilizations of such phenomenon. Recently the procedure of implementing both nanoliquid and porous medium has greeted massive consideration and has directed to ample researches in this domain. Nanoparticles disseminated in nanoliquid augment the effective conductivity while porous media upsurges the surface area in relation solid surface and liquid. Consequently it appears that utilizing both nanoliquid and porous media can raise the effectiveness of standard thermal system meaningfully [11].

Aforementioned analyses witness that nanoliquid and porous medium are considered for viscous liquid situation. Here we aimed to account porous medium aspect employing generalized Darcy relation for hydromagnetic nanoliquid-flow considering viscoelastic (second-grade) liquid. Such consideration is in fact the modification of Darcy expression through boundary features and inertia. Such characteristics cannot be overlooked at higher flow rate. Numerous investigators implemented this relation for flow analysis, for detail see [12-20]. Present research further includes double stratification, suction/injection, heat generation and convective conditions. The HAM [21-25] is opted to achieve non-linear convergent problems. Furthermore the meaningful variables arising in formulated problem are elucidated through graphs.

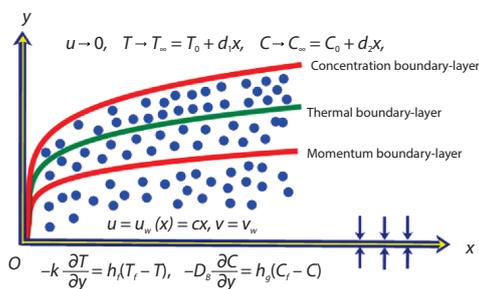


Figure 1. Physical configuration

Formulation

An incompressible viscoelastic (second-grade) liquid-flow by permeable stratified surface is formulated. Hydromagnetic characteristics are accounted for flow analysis. The Robin's type boundary conditions in addition double stratification are imposed at moving surface, fig. 1. Brownian diffusion, heat source and thermophoretic aspects are retained. By employing overhead suppositions, we have:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad (1)$$

$$\begin{aligned} u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + \frac{\alpha_1}{\rho_f} \left(u \frac{\partial^3 u}{\partial x \partial y^2} - \frac{\partial u}{\partial y} \frac{\partial^2 u}{\partial x \partial y} + v \frac{\partial^3 u}{\partial y^3} + \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial y^2} \right) = \\ = v \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B_0^2 u}{\rho_f} - \frac{v}{K} u - Fu^2 \end{aligned} \quad (2)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} + \tau \left[\frac{D_T}{T_\infty} \left(\frac{\partial T}{\partial y} \right)^2 + D_B \frac{\partial C}{\partial y} \frac{\partial T}{\partial y} \right] + \frac{Q}{(\rho c)_f} (T - T_\infty) \quad (3)$$

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial y^2} + D_B \frac{\partial^2 C}{\partial y^2} \quad (4)$$

$$\left\{ \begin{array}{l} u = u_w(x) = cx \\ v = v_w \\ -k \frac{\partial T}{\partial y} = h_f (T_f - T) \\ -D_B \frac{\partial C}{\partial y} = h_g (C_f - C) \end{array} \right\} \text{ at } y = 0 \text{ where } T_f = T_0 + a_1x \text{ and } C_f = C_0 + a_2x \quad (5)$$

$$\left\{ \begin{array}{l} u \rightarrow 0 \\ T \rightarrow T_\infty = T_0 + d_1x \\ C \rightarrow C_\infty = C_0 + d_2x \end{array} \right\} \text{ when } y \rightarrow \infty$$

Employing [25]:

$$\eta = y \sqrt{\frac{c}{\nu}}, \quad u = cx f'(\eta), \quad v = -\sqrt{c\nu} f(\eta), \quad \theta(\eta) = \frac{T - T_\infty}{T_f - T_0}, \quad \phi(\eta) = \frac{C - C_\infty}{C_f - C_0} \quad (6)$$

one obtains:

$$f''' + ff'' + \beta(2ff''' - f''^2 - ff^{iv}) - (\lambda + \text{Ha}^2) f' - (1 + F_r) f'^2 = 0 \quad (7)$$

$$\theta'' + \text{Pr}(f\theta' - f'\theta - S_1 f' + Nb\phi'\theta' + Nt\theta^2 + \delta\theta) = 0 \quad (8)$$

$$\phi'' + \frac{Nt}{Nb} \theta'' + \text{Sc}(f\phi' - f'\phi - S_2 f') = 0 \quad (9)$$

$$f = S, \quad f' = 1, \quad \theta' = -\gamma_1[1 - S_1 - \theta(\eta)]$$

$$\phi' = -\gamma_2[1 - S_2 - \phi(\eta)] \text{ at } \eta = 0 \quad (10)$$

$$f' \rightarrow 0, \quad \theta \rightarrow 0, \quad \phi \rightarrow 0 \text{ as } \eta \rightarrow \infty \quad (11)$$

The variables entering in eqs. (7)-(10) are delineated:

$$\lambda = \frac{\nu}{Kc}, \quad \beta = \frac{\alpha_1 c}{\mu}, \quad S = \frac{-v_w}{\sqrt{c\nu}}, \quad F_r = \frac{C_b x}{\sqrt{K}}, \quad C_b = \frac{C_b^*}{x}, \quad \text{Ha}^2 = \frac{\sigma B_0^2}{\rho_f c}$$

$$Nt = \frac{\tau D_T (T_f - T_0)}{T_\infty \nu}, \quad \text{Pr} = \frac{\nu}{\alpha}, \quad S_1 = \frac{d_1}{a_1}, \quad Nb = \frac{\tau D_B (C_f - C_0)}{\nu} \quad (12)$$

$$S_2 = \frac{d_2}{a_2}, \quad \text{Sc} = \frac{\nu}{D_B}, \quad \gamma_1 = \frac{h_f}{k} \sqrt{\frac{\nu}{c}}, \quad \delta = \frac{Q}{c(\rho c)_f}, \quad \gamma_2 = \frac{h_g}{D_B} \sqrt{\frac{\nu}{c}}$$

Local dimensional quantities (coefficient of drag-force, heat transfer rate, mass-transfer rate) are provided below:

$$C_{f_x} = \frac{\tau_w}{\rho u_w^2}, \quad \tau_w = \left[\mu \frac{\partial u}{\partial y} + \rho \alpha_1 \left(2 \frac{\partial u}{\partial x} \frac{\partial u}{\partial y} + u \frac{\partial^2 u}{\partial x \partial y} \right) \right]_{y=0} \quad (13a)$$

$$\text{Nu} = \frac{xq_w}{k(T_f - T_\infty)}, \quad q_w = -k \left(\frac{\partial T}{\partial y} \right)_{y=0} \quad (13b)$$

$$Sh = \frac{xq_m}{D_B(C_f - C_\infty)}, \quad q_w = -D_B \left(\frac{\partial C}{\partial y} \right)_{y=0} \tag{13c}$$

Coefficient of drag-force, $C_{fx}Re_x^{0.5}$, heat-transfer rate, $NuRe_x^{-0.5}$, and mass-transfer rate, $ShRe_x^{-1/2}$, in non-dimensional forms are:

$$C_{fx} Re_x^{0.5} = [1 + 3\beta f'(0)]f''(0) \tag{14}$$

$$\frac{Nu}{Re_x^{0.5}} = -\frac{1}{1 - S_1} \theta'(0) \tag{15}$$

$$\frac{Sh}{Re_x^{0.5}} = -\frac{1}{1 - S_2} \phi'(0) \tag{16}$$

where $Re_x = cx^2/\nu$.

Simulation procedure and outcomes

In the present article HAM is utilized to compute the non-linear problems, eqs. (7)-(11). This approach is based on semi-analytical technique which uses the concept of homotopy

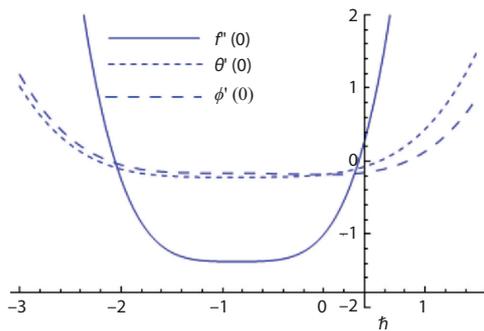


Figure 2. The h -curve plot of f , θ , and ϕ

to produce convergent solutions. To fulfill the purpose, one can witness the ranges of \tilde{h}_ϕ , \tilde{h}_θ , and \tilde{h}_f obtained from the HAM code developed in Wolfram MATHEMATICA 12.0.1. The said ranges from fig. 2 are $-1.40 \leq \tilde{h}_\phi \leq -0.55$, $-1.45 \leq \tilde{h}_\theta \leq -0.35$, and $-1.0 \leq \tilde{h}_f \leq -0.5$. Moreover, we also validate our convergent results by analyzing tab. 1. Convergence at 15th order approximation is developed, as shown in eqs. (7)-(9). An excellent agreement is achieved with [19], tab. 2. Effects of various parameters like Pr, Ha, S_1 , S_2 , δ , γ_1 , γ_2 , Nt , Nb , and Sc on $\theta(\eta)$, $\phi(\eta)$, $C_{fx}Re_x^{0.5}$, $NuRe_x^{-0.5}$, and $ShRe_x^{-0.5}$ are expounded in figs. 3-16.

Figure 3 is plotted to capture the effects of Nt on $\theta(\eta)$. This graph show that the enhancement of Nt results in the higher temperature. The variations of $\theta(\eta)$ against various values of Nb are displayed in fig. 4. The $\theta(\eta)$ rises as expected. This implies that the transportation of

Table 1. Convergent outcomes for distinctive order approximations considering $Nt = Ha = Nb = Fr = 0.1$, $S_2 = \beta_1 = \delta = S_1 = 0.2$, $\gamma_2 = \gamma_1 = 0.3$, $S = 0.4$, $\lambda = 0.5$, $Sc = 0.8$, and $Pr = 1.2$

Order of approximations	$-f''(0)$	$-\theta'(0)$	$-\phi'(0)$
1	1.2503	0.2065	0.1844
4	1.3731	0.2190	0.1649
9	1.3745	0.2194	0.1637
15	1.3745	0.2194	0.1637
25	1.3745	0.2194	0.1637
35	1.3745	0.2194	0.1637
40	1.3745	0.2194	0.1637

Table 2. Comparative values for $-f''(0)$ considering λ estimations when $F_r = Ha = S = \beta = 0.0$

	$-f''(0)$	$-f''(0)$
λ	[11]	Present
0.0	1.0000	1.0000
0.50	1.0198	1.0198
1.00	1.1180	1.1180

the nanoparticle upsurges for larger values of Nb . Such augmentation in heat transportation is owing to manifestation of Brownian diffusion, which causes exhilaration in nanoparticles. The deviation of $\theta(\eta)$ against S_1 , γ_1 , Pr , and δ is depicted in figs. 5-8. It can be noted that there is a temperature drop against increasing estimations of S_1 and Pr , whereas an opposite situation is witnessed for higher γ_1 and δ . Figure 9 is presented to capture the influence of Nt on $\phi(\eta)$. One can explicate that $\phi(\eta)$ is an increasing function of Nt . This rise is due to the generation of thermophoretic force for large Nt . This force aids nanoparticles movement in the less heated surroundings. The fluctuations of $\phi(\eta)$ for different Schmidt number are described in fig. 10. Diminution of $\phi(\eta)$ is countersigned for higher values of Schmidt number. This result is due to the reduction in mass diffusivity for greater Schmidt number. Figures 11-13 elucidates the trend of $\phi(\eta)$ vs. S_2 , γ_2 , and Nb . The S_2 and Nb resist $\phi(\eta)$ while γ_2 assist it. Figure 14 is plotted to illustrate the impact of Ha and λ on $C_{fx}Re_x^{0.5}$. It is highlighted that Ha and λ are assistive factors for the physical quantity $C_{fx}Re_x^{0.5}$. Characteristics of Nb , Nt , γ_2 , and Sc on $NuRe_x^{-0.5}$ and $ShRe_x^{-0.5}$ are delineated via figs. 15 and 16. As anticipated $NuRe_x^{-0.5}$ lessens for higher Nt and Nb while opposite trend is found when γ_2 and Sc are augmented.

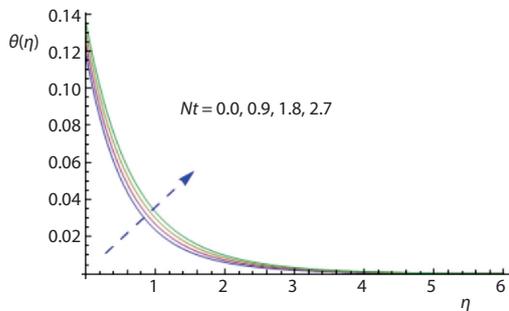


Figure 3. The θ via Nt

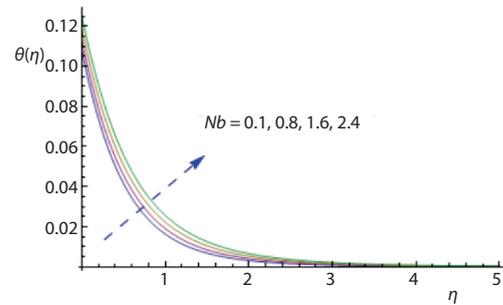


Figure 4. The θ via Nb

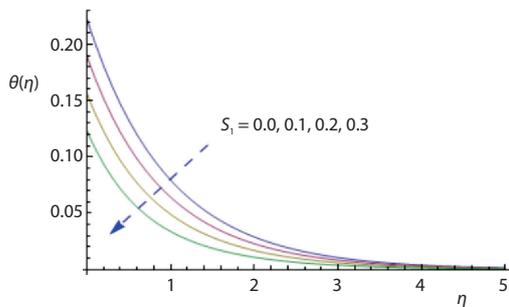


Figure 5. The θ via S_1

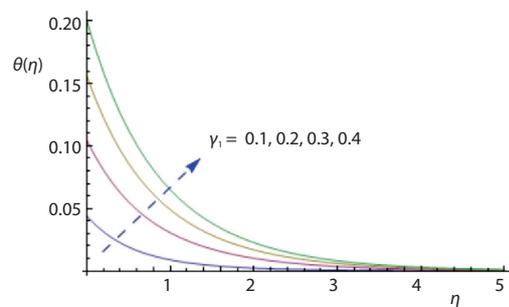


Figure 6. The θ via γ_1

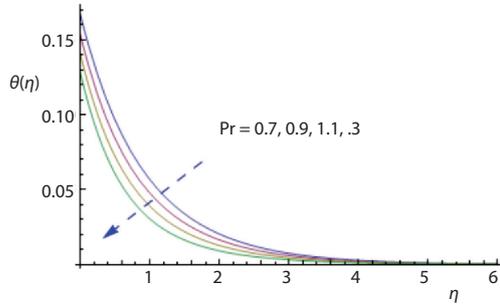


Figure 7. The θ via Pr

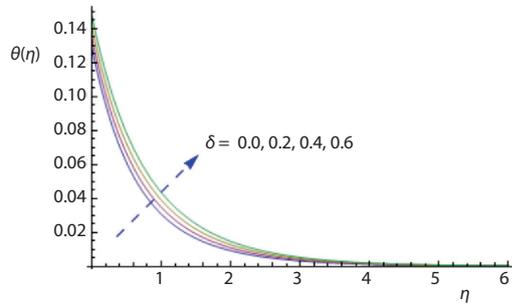


Figure 8. The θ via δ

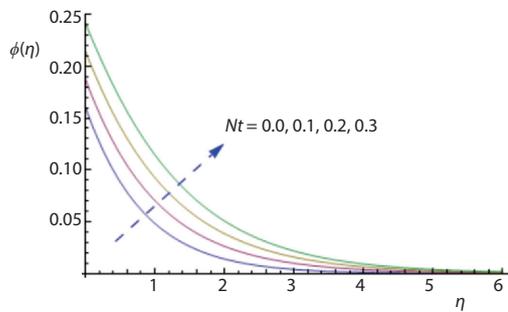


Figure 9. The ϕ via Nt

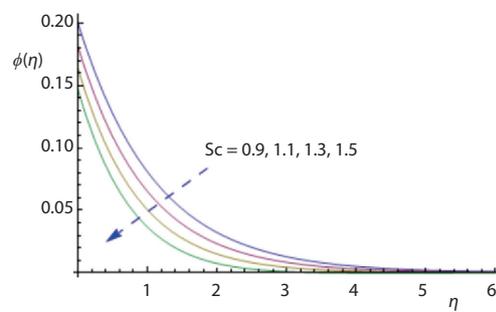


Figure 10. The ϕ via Sc

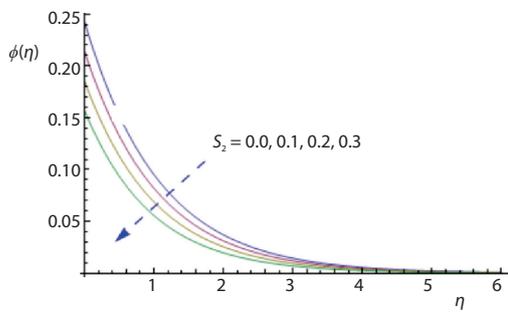


Figure 11. The ϕ via S_2

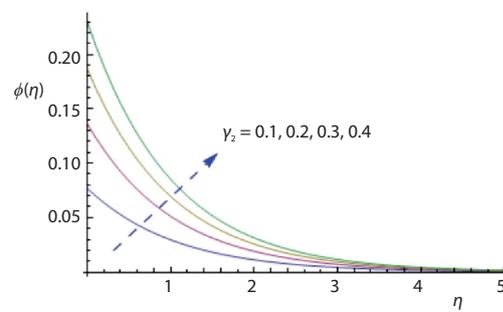


Figure 12. The ϕ via γ_2

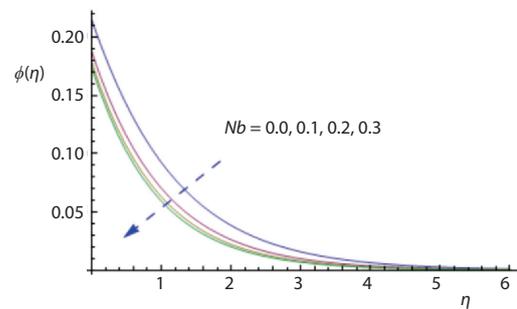


Figure 13. The ϕ via Nb

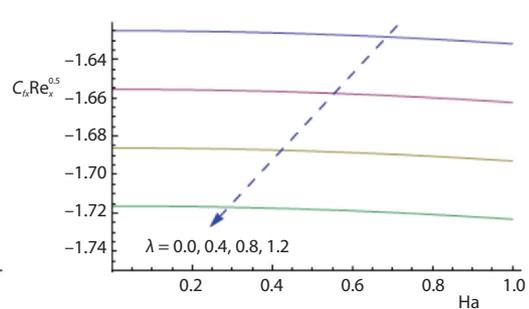


Figure 14. The $C_{f_x} Re_x^{0.5}$ via λ and Ha

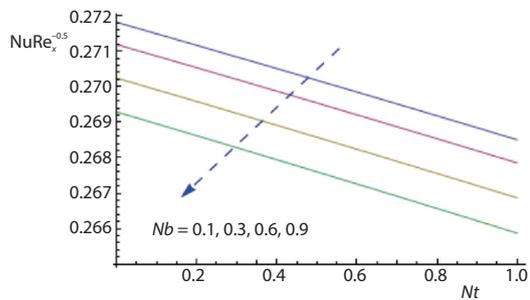


Figure 15. The $NuRe_x^{-0.5}$ via Nt and Nb

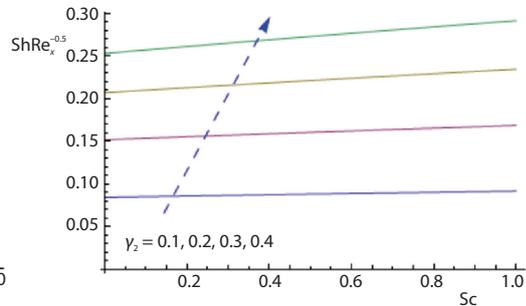


Figure 16. The $ShRe_x^{-0.5}$ via γ_2 and Sc

Conclusions

In the present work the MHD of a viscoelastic nanoliquid with non-Darcian properties is explored. The integration of convective conditions and stratifications with such fluid-flow problem make it even more novel. The resulting non-linear ODE is solved by famous HAM technique. The Nt and Nb are established as couple of assistive factors for $\theta(\eta)$ as compared to $NuRe_x^{-0.5}$. The $ShRe_x^{-0.5}$ is an increasing function of Sc and γ_2 . Concentration and temperature diminishes due to stratifications and convective conditions. It is worth-mentioning that modeled analysis corresponds to viscous nanoliquid situation when material parameter $\beta = 0$.

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Nomenclature

a_1, d_1, a_2, d_2 – non-dimensional constants
 B_0 – magnetic field intensity
 C – nanoparticle concentration
 C_b – drag coefficient
 C_b^* – coefficient of drag per length
 C_f – hot liquid concentration
 C_∞ – ambient liquid concentration
 C_0 – reference concentration
 $C_{fx}Re_x^{0.5}$ – non-dimensional drag force
 c – stretching rate
 D_B – Brownian movement coefficient
 D_T – thermophoresis diffusion coefficient
 F_r – local inertia coefficient
 $f'(\eta)$ – non-dimensional velocity
 Ha – Hartman number
 K – porous medium permeability
 k – thermal conductivity
 Nb – Brownian diffusion factor
 Nt – thermophoretic variable
 $NuRe_x^{-0.5}$ – non-dimensional heat transfer rate
 Pr – Prandtl number
 Q – uniform heat sink/source
 Re_x – Reynolds numbers
 S – mass-transfer parameter
 Sc – Schmidt number

$ShRe_x^{-0.5}$ – non-dimensional mass-transfer rate
 S_1 – thermal stratified variable
 S_2 – solutal stratified variable
 T – temperature
 T_f – hot liquid temperature
 T_0 – reference temperature
 T_∞ – ambient liquid temperature
 u_w – stretchable velocity
 u, v – components of velocity
 v_w – mass-transfer velocity
 x, y – space co-ordinates
 h_f, h_0, h_ϕ – auxiliary parameters

Greek symbols

α – thermal diffusivity
 α_1 – normal stress moduli
 β – second-grade liquid parameter
 γ_1 – thermal Biot number
 γ_2 – concentration Biot number
 δ – heat sink/source factor
 η – non-dimensional variable
 $\theta(\eta)$ – dimensionless temperature
 λ – porosity factor
 μ – dynamic viscosity
 ν – kinematic viscosity

ρ_f – base liquid density
 $(\rho c)_f$ – liquid heat capacity
 σ – electrical conductivity

τ – ratio of heat capacity
 $\phi(\eta)$ – dimensionless concentration

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