

THE EFFECTS OF SMALL AMOUNT OF HYDROGEN ADDITION ON PERFORMANCE AND EMISSIONS OF A DIRECT INJECTION COMPRESSION IGNITION ENGINE

by

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In this study, the effects of small amount of hydrogen addition into the intake of compression ignition engine on the performance and emissions characteristics of single cylinder, air cooled, direct injection, compression ignition engine were experimentally investigated. An electrolysis unit was built to produce hydrogen peroxide, which was then fed into the intake manifold of the compression ignition engine. The compression ignition engine was tested with different amount of hydrogen (0.15, 0.30, 0.45, and 0.60 Lpm) at different engine load (5%, 25%, 50%, 75%, and full load) and the constant speed, 2200 rpm. Experimental results show that increasing amount of hydrogen into the inlet air resulted to decrease in brake specific fuel and energy consumption while resulted to increase brake thermal efficiency at all load conditions due to uniformity in mixture formation and higher flame speed of hydrogen. The better combustion improved exhaust emission. However, exhaust temperature only increased for 0.6 Lpm hydrogen addition into the inlet air at higher loads resulting in higher quantity of nitrogen oxides formation.

Keywords: Diesel engine, electrolysis, hydrogen, engine performance, exhaust emissions

Introduction

Increasingly stringent emissions legislation on exhaust emissions, unfavorable effects of the emissions on human health and environment, and weakening of worldwide petroleum reserves afford strong encouragement for research on alternative fuels. As an alternative fuel, H₂ has great potential. Clean burning characteristics of H₂ and its better performance drives growing interest in H₂ such a fuel [1]. The compression ignition (CI) engines fueled with diesel and H₂ offers the potential of reduced emissions with improved performance [2]. Addition of H₂ can also result in extremely low smoke density (SD) and better thermal efficiency thereby reducing the fuel consumption however with a nominal power loss. Small amount addition of H₂ to a CI engine increases the H/C ratio of the entire fuel and decreases heterogeneity of a diesel fuel spray due to the high diffusivity of H₂ which makes better combustible mixture. It could also reduce the combustion duration due to its high speed of flame propagation [3-9].

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In an experimental investigation was conducted on a CI engine using port-injected H₂ as the primary fuel and direct in-cylinder diesel fuel injection to control ignition, Saravanan *et al.* [10] reported reductions in both NO_x and SD and increases in brake thermal efficiency (BTE) for dual-fuel operation compared with conventional CI engine operation. Varde and Varde [11] investigated effects of burning gaseous fuels together with diesel fuel in a naturally aspirated direct injection (DI) engine and detected that at light loads, the addition of H₂ reduced soot formation up to half of conventional diesel, while NO_x increased with increasing H₂-to-C ratio. Lee *et al.* [12] studied on H₂ mixed with the intake air by using injector and carbureting [13]. Electronic injectors using for H₂ have a superior control over the injection timing and injection duration with quicker response under high-speed operating conditions [14]. Elimination of problems like backfire and pre ignition with proper injection timing is the main advantage of H₂ injection over carbureted system [15]. In the study conducted by Tomita *et al.* [16], H₂ was mixed with the intake air of a DI-CI engine. It is reported that very low NO_x emissions were obtained when start of injection was advanced. As a result of less carbon content in the fuel, it was also observed that HC and CO emissions often reduced [17, 18]. An experimental research was employed by Saravanan and Nagarajan [19] on a stationary CI engine to improve performance and emissions. The NO_x emissions reduced one-fifth of the conventional case up to 90% H₂ enrichment at medium engine load. Conversely at full load, NO_x emissions increased slightly compared with conventional diesel operation, while SD reduced by about 50%. In another experimental investigation carried out by Saravanan *et al.* [20] was done on a CI engine using H₂ in the dual fuel mode. Experimental results showed an increase in BTE advance up to 30% with a significant reduction in NO_x compared with diesel.

However higher NO_x emissions that has an undesirable effect on environment is an obvious drawback of H₂-operated engines. The NO_x formation becomes significant when the combustion peak temperature is so high above 2200 K [21, 22]. Operating the H₂ engine with lean mixtures is one of the ways of reducing NO_x while keeping fuel economy better. That results in lower peak temperature that would slower the chemical reaction because of cooler combustion, which weakens the kinetics of NO_x formation [23, 24]. Using of H₂ in dual fuel mode with exhaust gas recirculation (EGR) technique also resulted in lower NO_x emissions with lower SD level and particulate matter [25]. The use of EGR is, therefore, believed to be most effective in improving exhaust emissions of H₂-operated engines.

The main disadvantage of using H₂ as a fuel for automobiles is on-board storage of H₂ and H₂ supply infrastructures are not available and need to be developed in near future [26-28]. One of the viable solutions to this problem is to generate H₂ on-board. Small amount of H₂ fumigation into the intake of engine by using an electrolysis unit positively affects engine performance and especially emissions. Gjirja *et al.* [29] was observed a decrease in NO_x when small amounts of hydrogen peroxide (H₂O₂) were fumigated into the intake of an engine using an electronic injector. Shirk *et al.* [30] conducted a sets of experiments to investigate the effects of fumigation gaseous H₂ to the intake of CI engines fueled with bio-diesel (B20). Results of experiments showed that NO_x emissions decreased slightly, exhaust temperature increased slightly, and efficiency changes were small. It can be concluded that H₂ fueled engine is not negatively impacted by the fumigation of small amounts of H₂.

From the literature review, the influence of small amount of addition H₂ into the intake of CI engine on the performance and emissions characteristics of CI engine has not been clearly studied. Therefore, these topics need to be investigated to make up for the deficiency in the literature. For this reason, in the present study, the effects of addition H₂ into the intake air of CI engine on the performance and emissions characteristics of single cylinder, air cooled, DI-CI

engine were experimentally investigated. An electrolysis unit was built to produce H_2O_2 , which was then fed into the intake manifold of the CI engine. The CI engine was tested with addition different amount of H_2 (0.15, 0.30, 0.45, and 0.60 Lpm) into the intake air at different engine load (5%, 25%, 50%, 75%, and full load) and the constant speed, 2200 rpm.

Experimental set-up

The Diesel engine used for the study was a DI, single cylinder; 4-stroke, air-cooled Lombardini 6 LD 400 engine. Bore and stroke of the engine are 86 mm and 68 mm, respectively. The compression ratio is 18:1. Maximum engine power and torque are 8 kW and 21 Nm, respectively. Fuel injection pressure and timing are 20 MPa and 20 °bTDC, respectively. The engine was loaded by an electrical dynamometer rated at 10 kW and 380 V. The load on the dynamometer was measured using a strain gauge load sensor. Accuracy of the load sensor is ± 2 N. An inductive pickup speed sensor was used to measure the speed of the engine. Accuracy of the speed sensor is ± 2 rpm. The fuel consumption was measured with a burette (10 and 20 ml volumes) and a stopwatch. The exhaust gas, lubricating oil, and air/fuel inlet temperatures were measured by type-K thermocouples. Accuracy of the thermocouples is ± 1 °C. The H_2 was generated by electrolyzing water using an O- H_2 generator machine.

The potassium hydroxide (KOH) water solution was used as a conductive electrolyte. By use of this system, the relation between the input voltage, KOH percentage and the produced H_2 gas was determined. The generated H_2 is then passed through a flow meter before it is introduced to the engine by the use of the air inlet manifold. The H_2 was passed through a non-return valve, preventing reverse flow of H_2 into the system. A flame arrestor was installed into the H_2 line in order to prevent flash-back into the H_2 -containing system. The H_2 from the flame arrestor was allowed inside the inlet manifold with a nozzle. The engine was started on neat diesel fuel and warmed up. The warm up period is assumed to end when the engine reaches the stabilized working condition (when the engine lubricating oil temperature reaches 75 ± 5 °C). The engine was operated at a constant speed of 2200 rpm obtained maximum torque with five different percentage of load (5%, 25%, 50%, 75%, and 100%). Under each load condition, the flow rate of diesel fuel and other parameters were first recorded without any induction of H_2 into the engine. Then, with no change in the experimental conditions, a small amount of H_2 (0.15, 0.30, 0.45, and 0.60 Lpm) was supplied to the intake manifold and the amount of diesel was arranged to obtain desired each load. In this study, the process of mixing air and H_2 is called as enrichment air with H_2 . After allowing the engine to reach steady-state conditions for about 10 min, engine parameters such as speed of operation, engine load, diesel fuel consumption, exhaust temperature were collected. Brake power, brake specific fuel consumption (BSFC), brake specific energy consumption (BSEC), and BTE were computed. Uncertainty of BSFC, BSEC, and BTE is $\pm 2.60\%$. Exhaust emissions like CO_2 , CO, HC, and NO_x were measured using an BOSCH-750 exhaust gas analyzer and SD was mea-

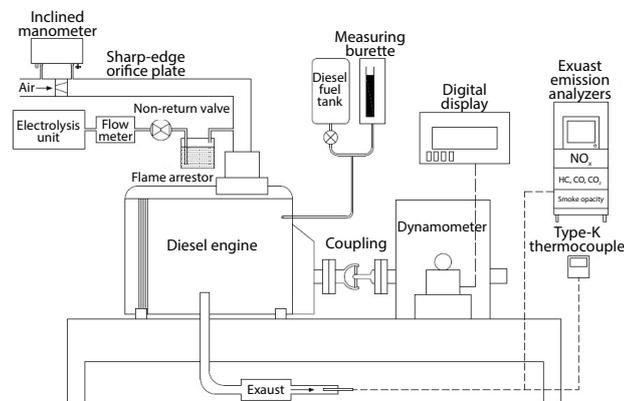


Figure 1. Schematic diagram of experimental set-up

sured using a smoke analyzer. Accuracy of CO_2 , CO, HC, and NO_x are $\pm 0.001\%$, $\pm 0.01\%$, ± 1 ppm, and ± 1 ppm, respectively. Each reading was replicated thrice to obtain a reasonable value. Schematic diagram of experimental set-up is plotted in fig. 1.

Results and discussion

Engine performance

Addition of H_2 into the intake air has a significant effect on the emission characteristics and performance of a CI engine because H_2 has excellent combustion, desirable emissions characteristics and other positive features. Therefore, in this study, the influence of H_2 addition on engine performance parameters such as BTE, BSFC, BSEC and emission characteristics such as NO_x , CO_2 , CO, HC, SD and exhaust gas temperature (EGT) of a single cylinder Diesel engine has been experimentally investigated. The experimental conditions were selected as follows: four engine loads (5%, 25%, 50%, 75%, and full load), 2200 rpm constant speed and four different amount of H_2 (0.15, 0.30, 0.45, and 0.60 Lpm).

Brake thermal efficiency

The BTE is defined as the ratio of the brake power to fuel consumption and lower heat value (LHV). The BTE indicates the ability of the combustion system and provides comparable means of assessing how efficient the energy in the fuel was converted to mechanical output [31]. The variation of BTE with respect to load for different amount of introduced H_2 is shown in fig. 2. Increasing engine load causes to increase in BTE values due to noticeably decline in BSFC for all fuel mixture. At 75% load, the maximum BTE for 0.60 Lpm H_2 enrichment is

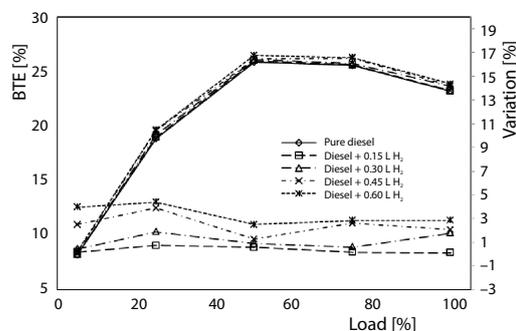


Figure 2. Variation of BTE

26.29% compared to 25.56% for pure diesel operation. It can be seen from fig. 2, 2.85% improvement is occurred in BTE. At full load, the highest BTE is found to be 23.88% for 0.60 Lpm H_2 enrichment compared to diesel of 23.21%. The increase in BTE is owing to the uniformity in mixture formation and higher flame speed of H_2 assists to have more complete combustion resulting in an improvement in BTE at all load conditions [32]. The best results in terms of BTE were obtained at 0.60 Lpm addition of H_2 .

Brake specific fuel consumption

The BSFC is defined as the ratio of the fuel consumption to the brake power [33]. The variation of BSFC with respect to engine load for the neat diesel fuel and the H_2 enrichments is presented in fig. 3(a). For all of the fuels, BSFC has the tendency to decrease with respect to increasing of engine load until it reaches a minimum value and then increases a small amount with further increase in engine load. One possible explanation for this decrease could be the higher percentage increase in the brake power with load as compared to fuel consumption.

As shown in fig. 3(a), the BSFC slightly decreased with increasing H_2 amount in the inlet mixture because of owing to the uniformity in mixture formation and higher flame speed of H_2 leads to better combustion resulting in an improvement in BSFC at all load conditions. At 75% load the minimum BSFC value is acquired 322.18 g/kWh for 0.60 Lpm H_2 enrichment compared to diesel of 331.35 g/kWh. At full load, the minimum value of BSFC is 354.73 g/kWh

at 0.60 Lpm H₂ flow rate compared to pure diesel 364.88 kg/kWh. On average for all engine loads, BSFC for 0.15, 0.30, 0.45, and 0.60 Lpm H₂ addition boosted by 0.22, 0.77, 1.72, and 2.44%, respectively, compared to those of pure diesel.

Brake specific energy consumption

The BSEC is described as multiplication of BSFC and LHV [34]. As shown in the fig. 3(b), the BSEC reduces with increasing engine loads because of noticeably diminishing BSFC for the all fuel mixtures. It is also observed from the fig. 3(b) that the BSEC for all of the H₂ addition conditions is lower than that of diesel. The lowest BSEC of 13.59 MJ/kWh is obtained for 0.60 Lpm H₂ enrichment compared to diesel of 14.08 MJ/kWh at 75% load. At full load, the BSEC for H₂ enriched engine is 15.08 MJ/kWh compared to diesel, which is 15.51 MJ/kWh. The reduction is 2.77% at full load for 0.60 Lpm H₂ enrichment. The reduction in BSEC is due to better mixing of H₂ in addition to assisting diesel during the combustion process [26]. The optimum BSEC was found to be at 0.60 Lpm H₂ enrichment.

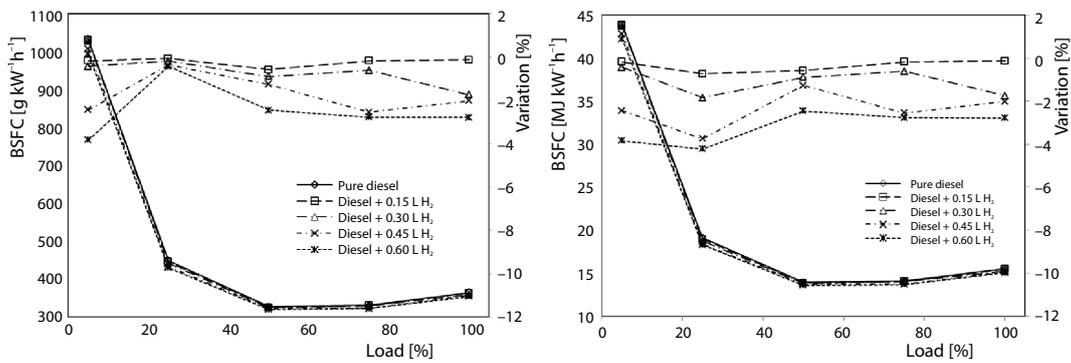


Figure 3. Variation of BSFC (a), and BSEC (b)

Exhaust gas temperature

Figure 4(a) depicts the variation of EGT with load. The EGT increases with increase in load. It is observed that the EGT for all H₂ enrichment conditions is higher than diesel at full load. At full load the maximum EGT was 599 °C at 0.60 Lpm H₂ enriched air mixture compared to diesel of 581 °C.

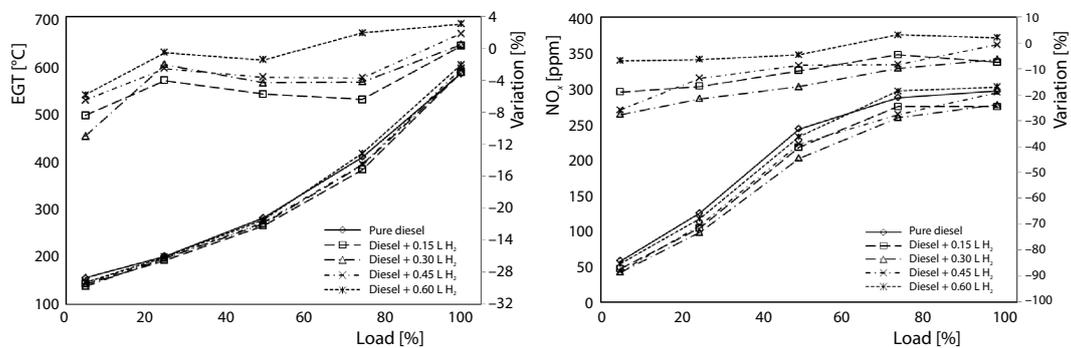


Figure 4. Variation of EGT (a), and NO_x emissions (b)

Exhaust emissions

Nitrogen oxides

The conversion of nitrogen and oxygen to NO_x is generated by the high combustion temperatures occurring within the burning fuel sprays controlled by local conditions. The NO_x is collective term used to refer to NO and NO_2 . The NO_x emissions form in the high temperature burned gas region, which is non-uniform, and formation rates are highest in the close to stoichiometric regions [34]. The variation of NO_x with the engine load for different amount of H_2 into the inlet air is presented in fig. 4(b).

The NO_x emissions increased with the increasing engine load because of increasing combustion temperature as shown in fig. 4(b). The NO_x emissions decreased for all H_2 enrichments at lower load condition. However at higher load conditions, NO_x emissions initially decreases slightly with the addition of H_2 into the inlet air until it reaches 0.45 Lpm value but it increases with more enhancement of the H_2 addition owing to better combustion leads to higher temperature resulting in an increase in NO_x emissions. The NO_x emission is found to be high, 296 ppm at 75% load for 0.60 Lpm H_2 enrichment compared to diesel of 287 ppm. At full load for 0.60 Lpm H_2 enrichment NO_x is found to be 302 ppm compared to diesel of 296 ppm. On average for all engine loads, NO_x emissions for 0.15, 0.30, 0.45, and 0.60 Lpm H_2 addition decreased by 11.68, 16.44, 11.42, and 2.53% compared to those of pure diesel, respectively.

Smoke density

Due to the heterogeneous nature of diesel combustion, there is a wide distribution of air/fuel ratios within the cylinder. The SD is attributed to either air/fuel mixtures that are too lean to autoignite or to support a propagating flame, or air/fuel mixtures that are too rich to ignite. Soot formation mainly takes place in the fuel-rich zone at high temperature and high pressure, especially within the core region of each fuel spray, and is caused by high temperature decomposition [31]. The variation of SD with the engine load for different H_2 enrichments is depicted in fig. 5(a). The formation of smoke strongly depends on the engine load. As the load increases, more fuel is injected, and this increases the formation of smoke. The results obtained in this study support this statement.

As seen in fig. 5(a), SD has tendency to decrease with the increasing fraction of H_2 into the inlet mixture. At 75% load in the 0.60 Lpm H_2 enriched condition is observed to be 40.41% compared to diesel of 44.14%. The lowest SD value of 6.29% is observed at 0.60 Lpm H_2 enrichment at 5% load. The H_2 forms a homogeneous air/fuel mixture rather than heterogeneous mixture unlike diesel resulting in a further reduction in SD. For all engine loads, SD for 0.15, 0.30, 0.45, and 0.60 Lpm H_2 addition diminished by 7.74, 16.10, 20.34, and 27.58% compared to those of pure diesel, respectively.

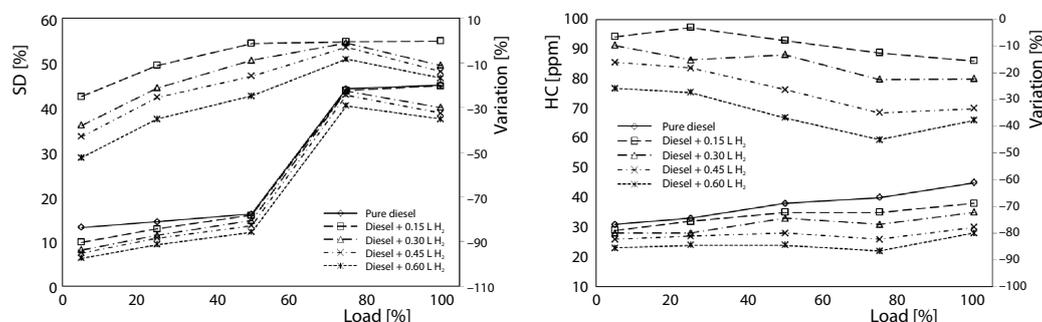


Figure 5. Variation of SD (a), and HC (b)

Hydrocarbon

The variation of HC with engine load for different percent H₂ into the inlet mixture is given in fig. 5(b). As shown in the figure, HC emission was steadily decreased when the amount of H₂ increased in the inlet air. This is also due to the uniformity in mixture formation and higher flame speed of H₂ leads to better combustion resulting in an improvement in HC emission at all load conditions [35]. At 75% load the HC is 22 ppm for the 0.60 Lpm H₂ enrichment compared to 40 ppm for diesel. At full load the H₂ enrichment results in a decrease in HC emission compared to neat diesel operated engine. For 0.60 Lpm H₂ operation it is 28 ppm compared to diesel of 45 ppm. On average, HC emissions for all engine loads for 0.15, 0.30, 0.45, and 0.60 Lpm H₂ addition decreased by 9.09, 16.54, 25.79, and 34.53% compared to those of pure diesel, respectively.

Carbon monoxide

The CO emissions in the exhaust represent lost chemical energy that is not fully used in the engine. Generally, CO emission is affected by the equivalence ratio, fuel type, combustion chamber design, atomization rate, start of injection timing, engine load, and speed. The most important among these parameters is the fuel type [31].

The variation of CO with engine load for the different amount of H₂ into the inlet air is presented in fig. 6(a). While the fuels are producing low amount of CO emission at light load levels, those are giving more emissions at high loading conditions. The CO emissions are found to be increasing with the increase in load. It is also observed from the figure that the CO emission of H₂ enrichment for all the operating parameters is lower than that of diesel. The CO emission for 0.60 Lpm H₂ enriched operation is 0.036% by volume compared to 0.047% by volume for neat diesel at 5% load. At full load the H₂ enrichment results an increase in CO emission compared to part load operations. The value of CO being 0.634% by volume for 0.60 Lpm H₂ enrichment compared to that of diesel of 0.980% by volume. For all engine loads, CO emissions for 0.15, 0.30, 0.45, and 0.60 Lpm H₂ addition decreased by 4.37, 12.61, 17.13, and 23.94% compared to those of pure diesel, respectively. The reduction in CO in H₂ enrichment conditions is due to the absence of carbon in H₂ fuel.

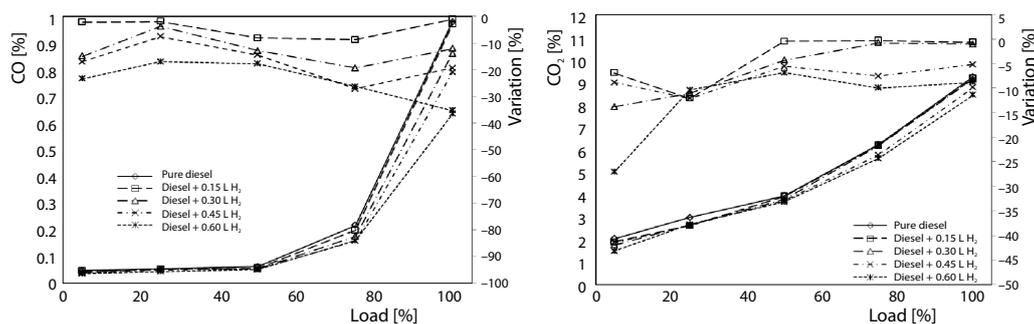


Figure 6. Variation of CO (a) and CO₂ (b) emissions

Carbon dioxide

The CO₂ emission is produced by complete combustion of fuel. Ideally, combustion of a HC should produce only CO₂ and water (H₂O) [36]. The variation of CO₂ with the engine load for different H₂ addition into inlet air is depicted in fig. 6(b). As expected, the CO₂ emission increases with the increasing load. The main reason of increasing of CO₂ with increasing load is

more fuel injected into the engine. The other reasons are increasing in combustion temperature and oxidization rates.

As seen in fig. 6(b), the CO₂ values are lesser for H₂ enriched conditions compared to neat diesel condition. The CO₂ for 0.60 Lpm H₂ enrichment is 5.60% by volume compared to 6.22% by volume for pure diesel at 75% load. At full load, the CO₂ for 0.60 Lpm H₂ enrichment is 8.42% by volume compared to 9.23% by volume for diesel. For all engine loads, CO₂ emissions decreased by 4.09, 6.21, 7.85, and 12.62% for 0.15, 0.30, 0.45, and 0.60 Lpm H₂ addition compared to those of neat diesel, respectively. The reasons of reduction in CO₂ concentration with H₂ addition into the inlet mixture are burning of H₂ supplies energy without bringing carbon into the engine and the improved thermal efficiency benefiting from the improved combustion [37].

Conclusions

In this study, the effects of addition H₂ into the intake air of CI engine on the performance and emissions characteristics of single cylinder, air cooled, DI-CI engine were experimentally investigated. An electrolysis unit was built to produce H₂, which was then fed into the intake manifold of the CI engine. The CI engine was tested with addition different amount of H₂ into the intake air (0.15, 0.30, 0.45, and 0.60 Lpm) at different engine load (5%, 25%, 50%, 75%, and full load) and the constant speed, 2200 rpm. From the experimental results, the following conclusions were made.

- Addition of H₂ into the intake air has a significant effect on the engine performance and emissions because H₂ has excellent effects on the fuel spray combustion.
- Increasing amount of H₂ into the inlet air resulted to decrease in BSFC and BSEC while resulted to increase BTE at all load conditions. This is probably the result of uniformity in mixture formation and higher flame speed of H₂ leads to better combustion. The best results in terms of BSFC, BSEC, and BTE were obtained at 0.60 Lpm addition of H₂.
- The NO_x emissions generally decreased for all H₂ enrichment conditions. However, combustion temperature only increased for 0.6 Lpm H₂ addition into the inlet air at higher loads. This caused to higher quantity of NO_x formation.
- The better uniformity in mixture formation with H₂ enrichment and higher flame speed of H₂ leads to better combustion resulting in an improvement in SD, HC, and CO emissions. The optimum emissions were found to be at 0.60 Lpm H₂ enrichment.
- The H₂ leads to more complete combustion. The CO₂ concentration are lesser for H₂ enriched conditions compared to neat diesel condition due to burning of H₂ supplies energy without bringing carbon into the engine and the improved thermal efficiency benefiting from the better combustion.

Consequently addition of small amount of H₂ produced by electrolysis into the inlet air of DI-CI engine results in improved performance level and generally lowered emission level compared to the case of neat diesel operation.

References

- [1] Garni, M. A., Simple and Reliable Approach for the Direct Injection of Hydrogen in Internal Combustion Engines at Low and Medium Pressures, *Int. J. Hydrogen Energy*, 20 (1995), 9, pp. 723-6
- [2] Das, L. M. Near-Term Introduction of Hydrogen Engines for Automotive and Agricultural Application, *Int. J. Hydrogen Energy*, 27 (2002), 5, pp. 479-87
- [3] Tsolakis, A., Megaritis, A., Partially Premixed Charge Compression Ignition Engine with on-Board H₂ Production by Exhaust Gas Fuel Reforming of Diesel and Biodiesel, *Int. J. Hydrogen Energy*, 30 (2006), 7, pp. 2448-2457

- [4] Syed, Y., Masood, M., Effect of Ignition Timing and Compression Ratio on the Performance of a Hydrogen-Ethanol Fuelled Engine, *Int. J. Hydrogen Energy*, 34 (2009), 16, pp. 6945-6950
- [5] Szwaja, S., Rogalinski, K. G., Hydrogen Combustion in a Compression Ignition Diesel Engine, *Int. J. Hydrogen Energy*, 34 (2009), 10, pp. 4413-4421
- [6] Porpatham, E., et al., Effect of Hydrogen Addition on the Performance of a Biogas Fuelled Spark Ignition Engine, *Int. J. Hydrogen Energy*, 32 (2007), 12, pp. 2057-2065
- [7] Kahraman, N., et al., Investigation of Combustion Characteristics and Emissions in a Spark-Ignition Engine Fuelled with Natural Gas-Hydrogen Blends, *Int. J. Hydrogen Energy*, 34 (2009), 2, pp. 1026-1034
- [8] Wang, J., et al., Study of Cycle-by-Cycle Variations of a Spark Ignition Engine Fueled with Natural Gas-Hydrogen Blends, *Int. J. Hydrogen Energy*, 33 (2008), 18, pp. 4876-4883
- [9] Bauer, C. G., Forest, T. W., Effect of Hydrogen Addition on the Performance of Methane-Fueled Vehicles, Part I: Effect on S. I. Engine Performance, *Int. J. Hydrogen Energy*, 26 (2001), 1, pp. 55-70
- [10] Saravanan, N., et al., Experimental Investigation of Hydrogen Port Fuel Injection in DI Diesel Engine, *Int. J. Hydrogen Energy*, 32 (2007), 16, pp. 4071-80
- [11] Varde, K. S., Varde, L. K., Reduction of Soot in Diesel Combustion with Hydrogen and Different H/C Gaseous Fuels, *Proceedings*, 5th World Hydrogen Energy Conference, Toronto, Ont., Canada, 1984
- [12] Lee, J. T., et al., An Investigation of a Cause of Backfire and its Control Due to Crevice Volumes in a Hydrogen Fueled Engine, *J. Eng. Gas Turbines Power*, 123 (2000), 1, pp. 204-210
- [13] Lee, J. T., et al., The Development of a Dual Injection Hydrogen Fueled Engine with High Power and High Efficiency, Fall Technical Conference of ASME-ICED, New Orleans, La., USA, 2002, pp. 323-333
- [14] Bailey, B., et al., Diethyl Ether (DEE) as a Renewable Diesel Fuel, *Proceedings*, SAE paper, 972978, 1997
- [15] Furuhashi, S., et al., Combustion Improvement in Hydrogen Fueled Engine, *Int. J. Hydrogen Energy*, 2 (1977), 3, pp. 329-40
- [16] Tomita, E., et al., Hydrogen Combustion and Exhaust Emissions Ignited with Diesel Oil in a Dual-Fuel Engine, SAE technical paper, 2001-01-3503, 2001
- [17] Senthil, K. M., Hydrogen Induction for Improving the Performance of a Vegetable Oil Fueled CI Engine, *Proceedings*, International Conference on WASTE to ENERGY, Jaipur, India, 2002
- [18] Senthil, K., Use of Hydrogen to Enhance the Performance of a Vegetable Oil Fuelled Compression Ignition Engine, *Int. J. Hydrogen Energy*, 28 (2003), 10, pp. 1143-1154
- [19] Saravanan, N., Nagarajan, G., An Experimental Investigation of Hydrogen-Enriched Air Induction in a Diesel Engine System, *Int. J. Hydrogen Energy*, 33 (2008), 6, pp. 1769-1775
- [20] Saravanan, N., et al., Combustion Analysis on a DI Diesel Engine with Hydrogen in Dual Fuel Mode, *Fuel*, 87 (2008), 17-18, pp. 3591-3599
- [21] Dec, J. E., A Conceptual Model of DI Diesel Combustion Based on Laser-Sheet Imaging, SAE paper, 970873, 1997
- [22] Dec, J. E., Kelly-Zion, P. L., The Effect of Injection Timing and Diluent Addition Latecombustion Soot Burnout in a DI Diesel Engine Based on Simultaneous 2-D Imaging of OH and Soot, SAE paper, 200001-0238, 2000
- [23] Michael, F. J., Brunt, H. R., The Calculation of Heat Release Energy from Engine Cylinder Pressure Data, SAE paper, 981052, 1998
- [24] Naber, J. D., Siebers, D. L., Hydrogen Combustion under Diesel Engine Conditions, *Int. J. Hydrogen Energy*, 23 (1998), 5, pp. 363-371
- [25] Saravanan, N., An Experimental Investigation on Hydrogen as a Dual Fuel for Diesel Engine System with Exhaust Gas Recirculation Technique, *Renew Energy*, 33 (2008), 3, pp. 422-427
- [26] Bari, S., Esmail, M. M., Effect of H₂/O₂ Addition in Increasing the Thermal Efficiency of a Diesel Engine, *Fuel*, 89 (2010), 2, pp. 378-383
- [27] Demirbas, A., Fuel Properties of Hydrogen, Liqueed Petroleum Gas (LPG), and Compressed Natural Gas (CNG) for Transportation, *Energy Sources*, 24 (2002), 7, pp. 601-610
- [28] Mitchell, W. et al., Dynamic Behavior of Gasoline Fuel Cell Electric Vehicles, *Journal of Power Sources*, 154 (2006), 2, pp. 489-496
- [29] Gijrja, S., et al., Experimental Investigation on the Hydrogen Peroxide Fumigation into the Inlet Duct of a Diesel Engine, SAE technical paper, 2001-01-1919, 2000
- [30] Shirk, M. G., et al., Haworth, Investigation of a H₂-Assisted Combustion System for a Light-Duty Diesel Vehicle, *Int. J. Hydrogen Energy*, 33 (2008), 23, pp. 7237-7244
- [31] Sayın, C., et al., Effect of Fuel Injection Timing on the Emissions of a Direct-Injection (DI) Diesel Engine Fueled with Canola Oil Methyl Ester-Diesel Fuel Blends, *Energy & Fuels*, 24, (2010), 4, pp. 2675-2682

- [32] Bari, S., Esmail, M. M., Effect of H₂/O₂ Addition in Increasing the Thermal Efficiency of a Diesel Engine, *Fuel*, 89 (2010), 2, pp. 378-383
- [33] Gumus, M., Sayin, *et al.*, Effect of Fuel Injection Timing on the Injection, Combustion, and Performance Characteristics of a Direct-Injection (DI) Diesel Engine Fueled with Canola Oil Methyl Ester-Diesel Fuel Blends, *Energy & Fuels*, 24 (2010), 5, pp. 3199-3213
- [34] Gumus, M., Evaluation of Hazelnut Kernel Oil of Turkish Origin as Alternative Fuel in Diesel Engines, *Renew Energy*, 33 (2008), 11, pp. 2448-2457
- [35] Gumus, M., Reducing Cold-Start Emission from Internal Combustion Engines by Means of Thermal Energy Storage System., *Appl Therm Eng.*, 29 (2009), 4, pp. 652-660
- [36] Gumus, M., Kasifoglu, S., Performance and Emission Evaluation of a Compression Ignition Engine Using a Biodiesel (Apricot Seed Kernel Oil Methyl Ester) and Its Blends with Diesel Fuel, *Biomass and Bioenergy*, 34 (2010), 1, pp. 134-139
- [37] Liew, C., *et al.*, An Experimental Investigation of the Combustion Process of Heavy-Duty Diesel Engine Enriched with H₂, *Int. J. Hydrogen Energy*, 35 (2010), 20, pp. 11357-11365