

## THE DIFFUSION MODEL OF FRACTAL HEAT AND MASS TRANSFER IN FLUIDIZED BED A Local Fractional Arbitrary Euler-Lagrange Formula

by

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*In this manuscript, the local fractional arbitrary Euler-Lagrange formula are utilized to address the diffusion model of fractal heat and mass transfer in a fluidized bed based on the Fick's law with local fractional vector calculus.*

*Key words:* diffusion equation, Fick' law, fluidized bed,  
local fractional vector calculus

### Introduction

A great interest in the theoretical study of heat transfer in fluidized beds has been shown during the past ten years. For example, the thermodynamics in fluidized bed with moist particles was proposed in [1-6]. The heat transfers of fluidized bed with geldart type-D particles, oxy-fuel fluidized bed boilers [7] and gas-solid fluidized beds [8] were presented. As one of models of fluidized beds [9, 10], the diffusion model was investigated by many authors, such as Tardos *et al.* [11], Hoebink *et al.* [12], Bukur *et al.* [13], Van Ballegooijen *et al.* [14], and Wang and Chen [15]. In [16], the hybrid Euler-Lagrange approach was considered to discuss the particle transport process of circulating fluidized bed. The Euler-Lagrange formula was applied to address the heat transfer of carrot cubes in a spout-fluidized-bed drier with moving boundaries [17].

In fact, the roughness surface of fractal materials can be designed [18, 19] to describe gas-solids flow in a circulating fluidized bed [20]. Fractal analysis of three-phase fluidized bed was suggested by Fan *et al.* [21] and Kikuchi *et al.* [22]. Recently, the local fractional vector calculus structured in [23] was utilized to describe fractal problems in various areas, such as quantum mechanics [24] and fluid mechanics [25-27]. The diffusion on solid [28] and its non-differentiable solution [29] were discussed.

The physical parameters of the classical diffusion model in [11-17] describing the heat and mass transfer in a fluidized bed is differentiable. However, the non-differentiable version of the diffusion model for the fractal heat and mass transfer in a fluidized bed is not considered. The present work develops the local fractional diffusion model of fractal heat and mass transfer in a fluidized bed and the local fractional arbitrary Euler-Lagrange formula.

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## The diffusion model of fluidized bed via local fractional derivative

### *Fractal mass transfer in fluidized bed*

Let the quantities  $\vec{J}(r, t)$  and  $\theta(r, t)$  be the flux of solute and the potential related to the concentration in fluidized bed, respectively. Due to the local fractional vector surface integral A (from Appendix), the integral form of the local fractional Fick's law in fluidized bed becomes:

$$\oint\oint \vec{J}(r, t) d\vec{S}^{(\beta)} = -\oint\oint D(\theta) \nabla^\alpha \theta(r, t) d\vec{S}^{(\beta)} \quad (1)$$

which leads to:

$$\oint\oint [\vec{J}(r, t) + D(\theta) \nabla^\alpha \theta(r, t)] d\vec{S}^{(\beta)} = 0 \quad (2)$$

where  $D(\theta)$  is a fractal diffusion coefficient in fluidized bed.

For any  $d\vec{S}^{(\beta)}$  in (2) the differential form of the local fractional Fick's law in fluidized bed can be written as [28]:

$$\vec{J}(r, t) = D(\theta) \nabla^\alpha \theta(r, t) \quad (3)$$

If  $D(\theta) = D$ , (4) changes [28]:

$$\vec{J}(r, t) = -D \nabla^\alpha \theta(r, t) \quad (4)$$

where  $D$  is a fractal diffusion coefficient in fluidized bed.

Using the local fractional volume integral B (from Appendix), the local fractional conservation of fractional mass in fluidized bed results in:

$$\frac{d^\alpha}{dt^\alpha} \iiint \theta(r, t) dV^{(\gamma)} = -\oint\oint \vec{J}(r, t) d\vec{S}^{(\beta)} \quad (5)$$

From (5) and C (from Appendix), we get:

$$\iiint \left[ \frac{d^\alpha \theta(r, t)}{dt^\alpha} + \nabla^\alpha \vec{J}(r, t) \right] dV^{(\gamma)} = 0 \quad (6)$$

For any  $dV^{(\gamma)}$  in (6) the differential form of local fractional conservation of fractional mass in fluidized bed is expressed as:

$$\frac{d^\alpha \theta(r, t)}{dt^\alpha} + \nabla^\alpha \vec{J}(r, t) = 0 \quad (7)$$

Submitting (4) into (7) gives the diffusion model for mass transfer in fluidized bed:

$$\frac{d^\alpha \theta(r, t)}{dt^\alpha} + \nabla^\alpha [-D \nabla^\alpha \theta(r, t)] = 0 \quad (8)$$

or

$$\frac{d^\alpha \theta(r, t)}{dt^\alpha} - D \nabla^{2\alpha} \theta(r, t) = 0 \quad (9)$$

subject to the initial-boundary conditions:

$$\theta(r, 0) = \theta_0(r) \quad (10)$$

$$-\nabla^\alpha \theta(r, t) \Big|_{S^{(\beta)}} = \eta[\theta_s(r, t) - \theta_e(r, t)], \quad t > 0 \quad (11)$$

where  $\theta_e(r, t)$  is the equilibrium moisture content in fluidized bed and  $\nabla^{2\alpha} = \nabla^\alpha \nabla^\alpha$ . If the fractal dimension  $\alpha$  is equal to 1, the diffusion model for fractal mass transfer in fluidized bed (9) becomes classical one [15, 17]. We notice that, using the fractal complex transform [30], the classical diffusion model for mass transfer in fluidized bed is transferred into (9).

#### *Fractal heat transfer in fluidized bed*

The local fractional Fourier law in fluidized bed can be written as [23]:

$$\phi(r, t) = -\mu \nabla^\alpha T(r, t) \quad (12)$$

where  $\mu$  is a constant and  $T(r, t)$  is a non-differentiable temperature at the point  $r \in V^{(\gamma)}$ , time  $t \in T$ .

The first law of thermodynamics in fractal media states [23]:

$$\iiint_{V^{(\gamma)}} \rho_\alpha c_\alpha \frac{\partial^\alpha T(r, t)}{\partial t^\alpha} dV^{(\gamma)} = \iint_{S^{(\beta)}} \phi(r, t) d\vec{S}^{(\beta)} \quad (13)$$

where  $\rho_\alpha$  and  $c_\alpha$  are the density and the specific heat of the fractal material, respectively.

Due to C (from Appendix) and (12), (13) can be rewritten as:

$$\iiint_{V^{(\gamma)}} \rho_\alpha c_\alpha \frac{\partial^\alpha T(r, t)}{\partial t^\alpha} dV^{(\gamma)} = \iiint_{V^{(\gamma)}} \mu \nabla^{2\alpha} T(r, t) dV^{(\gamma)} \quad (14)$$

which yields:

$$\iiint_{V^{(\gamma)}} \left[ \mu \nabla^{2\alpha} T(r, t) - \rho_\alpha c_\alpha \frac{\partial^\alpha T(r, t)}{\partial t^\alpha} \right] dV^{(\gamma)} = 0 \quad (15)$$

For any  $dV^{(\gamma)}$  in (6) fractal heat transfer in fluidized bed is suggested as:

$$\mu \nabla^{2\alpha} T(r, t) - \rho_\alpha c_\alpha \frac{\partial^\alpha T(r, t)}{\partial t^\alpha} = 0 \quad (16)$$

subject to the initial-boundary conditions:

$$T(r, 0) = T_0(r) \quad (17)$$

$$-\mu \nabla^\alpha T(r, t) = \zeta[T_s(r, t) - T_a(r, t)] - \lambda\{\nabla^\alpha [\rho \theta(r, t)]\}, \quad t > 0 \quad (18)$$

where  $\lambda$  is a medium property in fluidized bed. If the fractal dimension  $\alpha$  is equal to 1, the diffusion model for heat transfer in fluidized bed (16) becomes classical one [15, 17]. In another way, the classical diffusion model for mass transfer in fluidized bed is transferred into (16) using the fractal complex transform [30].

### The local fractional arbitrary Euler-Lagrange formula

The fractal mass transfer in fluidized bed is written in the weak form:

$$\iiint \left[ \frac{d^\alpha \theta(r, t)}{dt^\alpha} - D \nabla^{2\alpha} \theta(r, t) \right] \theta^*(r, t) dV^{(\gamma)} = 0 \quad (19)$$

which leads to:

$$\iiint \frac{d^\alpha \theta(r, t)}{dt^\alpha} \theta^*(r, t) dV^{(\gamma)} = - \oint \vec{J}(r, t) \theta^*(r, t) d\vec{S}^{(\beta)} \quad (20)$$

where  $\theta^*(r, t)$  is an arbitrary non-differentiable test function.

Using (4), we obtain the fractal mass transfer in fluidized bed:

$$\iiint \frac{d^\alpha \theta(r, t)}{dt^\alpha} \theta^*(r, t) dV^{(\gamma)} = \oint D \nabla^\alpha \theta(r, t) \theta^*(r, t) d\vec{S}^{(\beta)} \quad (21)$$

Following D (from Appendix), the right side of (21) can be written as:

$$\oint D \nabla^\alpha \theta(r, t) \theta^*(r, t) d\vec{S}^{(\beta)} = \iiint [D \theta^*(r, t) \nabla^{2\alpha} \theta(r, t) + D \nabla^\alpha \theta(r, t) \nabla^\alpha \theta^*(r, t)] dV^{(\gamma)} \quad (22)$$

which results in:

$$\iiint \frac{d^\alpha \theta(r, t)}{dt^\alpha} \theta^*(r, t) dV^{(\gamma)} = - \oint D \nabla^\alpha \theta(r, t) \theta^*(r, t) d\vec{S}^{(\beta)} + \iiint D \nabla^\alpha \theta(r, t) \nabla^\alpha \theta^*(r, t) dV^{(\gamma)} \quad (23)$$

such that, using (11), we have the local fractional arbitrary Euler-Lagrange formula of fractal mass transfer in fluidized bed:

$$\begin{aligned} \iiint \frac{d^\alpha \theta(r, t)}{dt^\alpha} \theta^*(r, t) dV^{(\gamma)} &= \oint \eta [\theta_s(r, t) - \theta_e(r, t)] \theta^*(r, t) d\vec{S}^{(\beta)} + \\ &+ \iiint D \nabla^\alpha \theta(r, t) \nabla^\alpha \theta^*(r, t) dV^{(\gamma)} \end{aligned} \quad (24)$$

The weak form of the heat transfer in fluidized bed reads as:

$$\iiint \left[ \mu \nabla^{2\alpha} T(r, t) - \rho_\alpha c_\alpha \frac{\partial^\alpha T(r, t)}{\partial t^\alpha} \right] T^*(r, t) dV^{(\gamma)} = 0 \quad (25)$$

where  $T^*(r, t)$  is an arbitrary non-differentiable test function.

From (25) we have:

$$\iiint T^*(r, t) \mu \nabla^{2\alpha} T(r, t) dV^{(\gamma)} = \iiint \rho_\alpha c_\alpha T^*(r, t) \frac{\partial^\alpha T(r, t)}{\partial t^\alpha} dV^{(\gamma)} \quad (26)$$

From D, the left side of (26) can be written as:

$$\iiint T^*(r, t) \mu \nabla^{2\alpha} T(r, t) dV^{(\gamma)} = \oint_{S^{(\beta)}} T^*(r, t) \mu \nabla^\alpha T(r, t) d\vec{S}^{(\beta)} -$$

$$-\iiint_{V^{(\gamma)}} \mu \nabla^\alpha T(r, t) \nabla^\alpha T^*(r, t) dV^{(\gamma)} \quad (27)$$

which, applying (18), yields:

$$\begin{aligned} \iiint T^*(r, t) \mu \nabla^{2\alpha} T(r, t) dV^{(\gamma)} &= -\iint_{S^{(\beta)}} T^*(r, t) \left\{ \varsigma [T_s(r, t) - T_a(r, t)] - \lambda \{D \nabla^\alpha [\rho \theta(r, t)]\} \right\} dS^{(\beta)} - \\ &\quad - \iiint_{V^{(\gamma)}} \mu \nabla^\alpha T(r, t) \nabla^\alpha T^*(r, t) dV^{(\gamma)} \end{aligned} \quad (28)$$

Submitting (28) into (26), we obtain:

$$\begin{aligned} \iiint \rho_\alpha c_\alpha T^*(r, t) \frac{\partial^\alpha T(r, t)}{\partial t^\alpha} dV^{(\gamma)} &= \\ = -\iint_{S^{(\beta)}} T^*(r, t) \left\{ \varsigma [T_s(r, t) - T_a(r, t)] - \lambda \{D \nabla^\alpha [\rho \theta(r, t)]\} \right\} d\bar{S}^{(\beta)} - \\ &\quad - \iiint_{V^{(\gamma)}} \mu \nabla^\alpha T(r, t) \nabla^\alpha T^*(r, t) dV^{(\gamma)} \end{aligned} \quad (29)$$

which is the local fractional arbitrary Euler-Lagrange formula of fractal heat transfer in fluidized bed.

### Concluding remarks

From pure mathematical view point, the local fractional diffusion model of fractal heat and mass transfer in fluidized bed is investigated in the framework of the local fractional vector calculus. Using the local fractional Gauss and Green theorems of the fractal vector field and considering an arbitrary non-differentiable test function, the local fractional arbitrary Euler-Lagrange formula of fractal heat and mass transfer in fluidized bed are also discussed. This result is an extended version of the arbitrary Euler-Lagrange formula using the non-differentiable characteristics of the functions in the field.

### Appendix

The local fractional vector surface integral of  $\vartheta(r)$  on fractal surface  $\bar{S}^{(\beta)}$  is defined as [23, 25, 27]:

$$\iint \vartheta(r_P) d\bar{S}^{(\beta)} = \lim_{N \rightarrow \infty} \sum_{P=1}^N \vartheta(r_P) \vec{n}_P \Delta \bar{S}_P^{(\beta)} \quad (A)$$

with  $N$  elements of area with a unit normal local fractional vector  $\vec{n}_P$ ,  $\Delta \bar{S}_P^{(\beta)} \rightarrow 0$  as  $N \rightarrow \infty$  for  $\beta = 2\alpha$ .

The local fractional volume integral of  $\vartheta(r)$  on fractal volume  $V^{(\gamma)}$  is defined as [23, 25, 27]:

$$\iiint \vartheta(r_P) dV^{(\gamma)} = \lim_{N \rightarrow \infty} \sum_{P=1}^N \vartheta(r_P) \Delta V_P^{(\gamma)} \quad (B)$$

with  $N$  elements of volume  $\Delta V_P^{(\gamma)} \rightarrow 0$  as  $N \rightarrow \infty$  for  $\gamma = 3\beta/2 = 3\alpha$ .

For  $\gamma = 3\beta/2 = 3\alpha$ ,  $1 > \alpha > 0$ , the local fractional Gauss theorem of the fractal vector field reads as [23, 25, 27]:

$$\iiint_{V^{(\gamma)}} \nabla^\alpha g dV^{(\gamma)} = \iint_{S^{(\beta)}} g d\bar{S}^{(\beta)} \quad (C)$$

For  $\gamma = 3\beta/2 = 3\alpha$ ,  $1 > \alpha > 0$ , the local fractional Green theorem of the fractal vector field states [23, 25]:

$$\iint_{S^{(\beta)}} \theta \nabla^\alpha g d\bar{S}^{(\beta)} = \iiint_{V^{(\gamma)}} (\theta \nabla^{2\alpha} g + \nabla^\alpha g \nabla^\alpha \theta) dV^{(\gamma)} \quad (D)$$

## Nomenclature

$c_a$	– specific heat
$D$	– a fractal diffusion coefficient
$r$	– space co-ordinates, [m]
$T(r, t)$	– temperature, [K]
$t$	– time, [s]

<i>Greek symbols</i>	
$\alpha$	– time fractal dimensional order, [-]
$\theta(r, t)$	– concentration, [-]
$\rho_a$	– density

## References

- [1] Syahrul, S., et al., Thermodynamic Modeling of Fluidized Bed Drying of Moist Particles, *International Journal of Thermal Sciences*, 42 (2003), 7, pp. 691-701
- [2] Dincer, I., Sahin, A. Z., A New Model for Thermodynamic Analysis of a Drying Process, *International Journal of Heat and Mass Transfer*, 474 (2004), 4, pp. 645-652
- [3] Mohideen, M. F., et al., Heat Transfer in a Swirling Fluidized Bed with Geldart Type-D Particles, *Korean Journal of Chemical Engineering*, 29 (2012), 7, pp. 862-867
- [4] Hristov, J. Y., Scaling of Permeabilities and Friction Factors of Homogeneously Expanding Gas-Solids Fluidized Beds: Geldart's A Powders and Magnetically Stabilized Beds, *Thermal Science*, 10 (2006), 1, pp. 19-44
- [5] Hristov, J., Magnetic Field Assisted Fluidization – A Unified Approach Part 7, Mass Transfer: Chemical Reactors, Basic Studies and Practical Implementations Thereof, *Reviews in Chemical Engineering*, 25 (2009), 1-2-3, pp. 1-254
- [6] Hristov, J., Magnetic Field Assisted Fluidization – A Unified Approach. Part 8. Mass Transfer: Magnetically Assisted Bioprocesses, *Reviews in Chemical Engineering*, 26 (2010), 3-4, pp. 55-128
- [7] Bolea, I., et al., Heat Transfer in the External Heat Exchanger of Oxy-Fuel Fluidized Bed Boilers, *Applied Thermal Engineering*, 66 (2014), 1, pp. 75-83
- [8] Patil, A. V., et al., A Study of Heat Transfer in Fluidized Beds Using an Integrated DIA/PIV/IR Technique, *Chemical Engineering Journal*, 259 (2015), Jan., pp. 90-106
- [9] Molerus, O., Wirth, K. E., *Heat Transfer in Fluidized Beds*, Springer, 2015
- [10] Kim, S. D., Kang, Y., Heat and Mass Transfer in Three-Phase Fluidized-Bed Reactors – an Overview, *Chemical Engineering Science*, 52 (1997), 21, pp. 3639-3660
- [11] Tardos, G., et al., Diffusional Filtration of Dust in a Fluidized Bed, *Atmospheric Environment*, 10 (1976), 5, pp. 389-394
- [12] Hoebink, J. H. B. J., Rietema, K., Drying Granular Solids in Fluidized Bed-I: Description on Basis of Mass and Heat Transfer Coefficients, *Chemical Engineering Science*, 35 (1980), 10, pp. 2135-2139
- [13] Bukur, D. B., Amundson, N. R., Fluidized Bed Char Combustion Diffusion Limited Models, *Chemical Engineering Science*, 36 (1981), 7, pp. 1239-1256
- [14] Van Ballegooijen, W. G. E., et al., Modeling Diffusion-Limited Drying Behaviour in a Batch Fluidized Bed Dryer, *Drying Technology*, 15 (1997), 3-4, pp. 837-85
- [15] Wang, H. Z., Chen, G., Heat and Mass Transfer in Batch Fluidized-Bed Drying of Porous Particles, *Chemical Engineering Science*, 55 (2000), 10, pp. 1857-1869
- [16] Adamczyk, W. P., et al., Modeling Oxy-Fuel Combustion in a 3D Circulating Fluidized Bed Using the Hybrid Euler-Lagrange Approach, *Applied Thermal Engineering*, 71 (2014), 1, pp. 266-275

- [17] Białobrzewski, I., et al., Heat and Mass Transfer during Drying of a Bed of Shrinking Particles – Simulation for Carrot Cubes Dried in a Spout-Fluidized-Bed Drier, *International Journal of Heat and Mass Transfer*, 51 (2008), 19, pp. 4704-4716
- [18] Pfeifer, P., Fractal Dimension as Working Tool for Surface-Roughness Problems, *Applications of Surface Science*, 18 (1984), 1, pp. 146-164
- [19] Gagnepain, J. J., Roques-Carmes, C., Fractal Approach to Two-Dimensional and Three-Dimensional Surface Roughness, *Wear*, 109 (1986), 1, pp. 119-126
- [20] Bai, D., et al., Fractal Characteristics of Gas-Solids Flow in a Circulating Fluidized Bed, *Powder technology*, 90 (1997), 3, pp. 205-212
- [21] Fan, L. T., et al., Stochastic Analysis of a Three-Phase Fluidized Bed: Fractal Approach, *AIChE Journal*, 36 (1990), 10, pp. 1529-1535
- [22] Kikuchi, R., et al., Fractal Aspect of Hydrodynamics in a Three-Phase Fluidized Bed, *Chemical Engineering Science*, 51 (1996), 11, pp. 2865-2870
- [23] Yang, X. J., *Advanced Local Fractional Calculus and its Applications*, World Science, New York, USA, 2012
- [24] Yang, X. J., et al., Mathematical Aspects of the Heisenberg Uncertainty Principle within Local Fractional Fourier Analysis, *Boundary Value Problems*, (2013), May, pp. 1-16
- [25] Yang, X. J., et al., Systems of Navier-Stokes Equations on Cantor Sets, *Mathematical Problems in Engineering*, 2013 (2013), ID 769724
- [26] Yang, X. J., et al., Modeling Fractal Waves on Shallow Water Surfaces via Local Fractional Korteweg-de Vries Equation, *Abstract and Applied Analysis*, 2014 (2014), ID 278672
- [27] Zhang, Y., et al., On a Local Fractional Wave Equation under Fixed Entropy Arising in Fractal Hydrodynamics, *Entropy*, 16 (2014), 12, pp. 6254-6262
- [28] Hao, Y. J., et al., Helmholtz and Diffusion Equations Associated with Local Fractional Derivative Operators Involving the Cantorian and Cantor-Type Cylindrical Coordinates, *Advances in Mathematical Physics*, 2013 (2013), ID 754248
- [29] Cao, Y., et al., Local Fractional Functional Method for Solving Diffusion Equations on Cantor Sets, *Abstract and Applied Analysis*, 2014 (2014), ID 803693
- [30] Yang, X. J., et al., Transport Equations in Fractal Porous Media within Fractional Complex Transform Method, *Proceedings of the Romanian Academy, Series A*, 14, (2013), 4 pp. 287-292