UNSTEADY FLOW AND HEAT TRANSFER OF JEFFREY FLUID OVER A STRETCHING SHEET

by

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The boundary layer flow and heat transfer of an incompressible Jeffrey fluid have been investigated. The analytic solutions of the arising differential system have been computed by homotopy analysis method. The dimensionless expressions for wall shear stress and surface heat transfer are also derived. Exact solutions of the momentum equation and numerical solutions of the dimensionless energy equations have been obtained for the steady-state case. The results indicate an increase in the velocity and the boundary layer thickness by increasing the elastic parameter (Deborah number) for a Jeffrey fluid.

Key words: unsteady flow, heat transfer, analytic solution, viscous dissipation

Introduction

Interest in the boundary layer flows of non-Newtonian fluids has increased due to the applications in science and engineering including thermal oil recovery, food and slurry transportation, polymer and food processing, etc. A variety of non-Newtonian fluid models have been proposed in the literature keeping in view of their several rheological features. In these fluids, the constitutive relationships between stress and rate of strain are much complicated in comparison to the Navier-Stokes equations. There is one subclass of non-Newtonian fluids known as Jeffrey fluid [1-4] which has been attracted much by the researchers in view of its simplicity. This fluid model is capable of describing the characteristics of relaxation and retardation times.

Heat transfer in the flows induced by the stretching surfaces has several applications. In fact the production of sheeting material is involved in various manufacturing processes and includes both metal and polymer sheets.

The rate of heat transfer over a surface has a pivotal role in the quality of final product. Industrial applications include fibers spinning, hot rolling, manufacturing of plastic and rubber sheet, continuous casting and glass blowing. Crane [5] studied the boundary layer flow of an incompressible viscous fluid towards a linear stretching sheet. An exact similarity solution for the
dimensionless differential system was obtained. Such closed form similarity solution has been obtained for several other features like viscoelasticity, magnetohydrodynamics, suction, porosity, and heat and mass transfer [6, 7, 8, 9]. Andersson et al. [10] discussed the slip effects on the flow of a viscous fluid over a stretching sheet. Axisymmetric flow of viscous fluid over a stretching sheet has been examined by Ariel [11]. Analytic solutions valid for large and small values of slip parameter have been obtained. Abbas and Hayat [12] provided an analytic solution for stagnation slip flow and heat transfer towards a stretching sheet by homotopy analysis method (HAM). Combined effects of slip and heat transfer on the flow of viscoelastic fluid were analyzed by Hayat et al. [13]. A homotopy solution valid for all values of slip parameter was obtained. Effect of suction on the 2-D and axisymmetric flows in the presence of partial slip has been examined by Wang [14]. Liao [15] presented the analytic solution for magnetohydrodynamic boundary layer flow of a power-law fluid towards a stretching surface. Dimensionless expressions for skin friction coefficient have been thoroughly addressed. A literature survey reveals significant research has been conducted on the steady boundary layer flows. However the time-dependent boundary layer flows have been scarcely studied. Devi et al. [16] numerically investigated the unsteady mixed convection stagnation-point flow towards a stretching surface. Andersson et al. [17] examined the heat transfer characteristics on the flow induced by an unsteady stretching sheet. Nazar et al. [18] discussed the unsteady boundary layer rotating flow due to a stretching surface. Liao [19] performed an analytic treatment of the unsteady boundary layer flow of a viscous fluid over a stretching surface. Mukhopadhyay [20] examined the effect of thermal radiation on the unsteady mixed convection flow and heat transfer bounded by a porous stretching surface embedded in a porous medium.

The present work deals with the analysis of unsteady boundary layer flow and heat transfer of Jeffrey fluid. Following Crane [5], an exact solution for the dimensionless momentum equation has been obtained for the steady-state case. However the energy equation has been solved numerically by MATHEMATICA. HAM has been employed to obtain the analytic solutions for all the dimensionless time \(0 \leq \tau \leq \infty\) in the whole spatial domain \(0 \leq \eta \leq \infty\). This method has been successfully applied to various interesting problems [21-30]. Graphs are portrayed to gain physical insight towards the embedding physical parameters.

Mathematical model

We consider the unsteady incompressible flow of a Jeffery fluid past a stretching sheet situated at \(y = 0\). The x- and y-axes are taken along and perpendicular to the sheet, respectively, and the flow is confined to \(y \geq 0\). It is assumed that the velocity of the stretching sheet is \(u_o(x) = ax\), where \(a\) is a positive (stretching sheet) constant. The viscous dissipation effects are retained. The boundary layer equations governing the unsteady flow and heat transfer of a Jeffrey fluid are:

\[
\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}
\]

\[
\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + \nu \frac{\partial u}{\partial y} = \frac{\nu}{1 + \lambda_2} \left[ \frac{\partial^2 u}{\partial y^2} + \lambda_1 \left( \frac{\partial^3 u}{\partial x \partial y^3} + \frac{\partial}{\partial x} \left( \frac{\partial^2 u}{\partial y^2} \frac{\partial}{\partial x} \right) - \frac{\partial^2 u}{\partial x \partial y^2} - \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial y^2} + \frac{\partial u}{\partial y} \frac{\partial^2 u}{\partial x \partial y} + \nu \frac{\partial^3 u}{\partial y^3} \right) \right] \tag{2}
\]
The boundary conditions are:

\[ t < 0: \quad v = 0, \quad u = 0, \quad T = T_w \quad \text{for any} \ x \ \text{and} \ y \]
\[ t \geq 0: \quad u = ax, \quad v = 0, \quad T = T_w \quad \text{at} \ y = 0, \]
\[ u \to 0, \quad T \to T_w, \quad \text{as} \ y \to \infty \]

in which \( u \) and \( v \) are the velocity components along x- and y-directions, respectively, \( \rho \) – the fluid density, \( \nu = \mu / \rho \) – the kinematic viscosity, \( T \) – the fluid temperature, \( \alpha \) – the thermal diffusivity, \( C_p \) – the specific heat, \( \lambda_2 \) – the ratio of relaxation and retardation time, and \( \lambda_1 \) – the relaxation time. Introducing [5]:

\[ \eta = \sqrt{\frac{\alpha}{\nu}} y, \quad u = axf'(\eta, \xi), \quad v = -\sqrt{\alpha \nu} \xi f(\eta, \xi), \]
\[ \xi = 1 - \exp[-\tau], \quad \tau = at, \quad \theta(\eta, \xi) = \frac{T - T_w}{T_w - T_w} \]

Equation (1) is automatically satisfied and eqs. (2)-(4) can be written as:

\[ \xi - \beta(1 - \xi)f'' + (1 + \lambda_2) \left[ \xi(1 - \xi) \left( \frac{\eta}{2} f'' - \xi f'' + \frac{\xi f''}{2} \right) - \xi^2 (f''^2 - ff'^2) \right] + \]
\[ + \beta \xi(1 - \xi) \frac{\partial f''}{\partial \xi} - \frac{\eta}{2} (1 - \xi) f'' + \xi (f''^2 - ff'^2) = 0 \]  
\[ (9) \]
\[ \xi \theta' + \Pr \xi(1 - \xi) \left( \frac{\eta}{2} \theta' - \xi \frac{\partial \theta}{\partial \xi} \right) + \Pr Ec \beta \xi \frac{\partial \theta}{\partial \xi} + \frac{\Pr Ec \beta}{1 + \lambda_2} \left[ \xi f'' + (1 - \xi) \left( \xi f'' + \frac{\xi f''}{2} \right) \right] = 0 \]
\[ f(0, \xi) = 0, \quad f'(0, \xi) = 1, \quad \theta(0, \xi) = 1, \quad f'(\infty, \xi) = 0, \quad \theta(\infty, \xi) = 0 \]

where \( \Pr \) is the Prandtl number, \( Ec \) – the Eckert number and \( \beta \) – the Deborah number which are defined by:

\[ \Pr = \frac{\nu}{\alpha}, \quad \beta = a\lambda_1, \quad Ec = \frac{(u_w)^2}{C_p(T_w - T_w)} \]

It is worth mentioning here that \( Ec > 0 \) corresponds to the heated wall \( (T_w > T_w) \) and corresponds to the case when the viscous dissipation term in the energy eq. (3) is neglected.

The skin friction coefficient \( C_f \) and local Nusselt number \( Nu_x \) are:

\[ C_f = \frac{\tau_w}{\rho u_w^2}, \quad Nu_x = \frac{\lambda q_w}{k(T_w - T_w)} \]  
\[ (10) \]

where the wall skin friction \( \tau_w \) and the heat transfer \( q_w \) from the plate are given by:
In view of eq. (5), the above expressions give:

\[
\begin{align*}
\tau_w &= \frac{\mu}{1 + \lambda_2} \left[ \frac{\partial u}{\partial y} + \lambda_1 \left( \frac{\partial^2 u}{\partial y \partial t} + u \frac{\partial^2 u}{\partial y \partial x} + v \frac{\partial^2 u}{\partial y^2} \right) \right]_{y=0} \\
q_w &= -k \left( \frac{\partial T}{\partial y} \right)_{y=0}
\end{align*}
\]  

(11) (12)

In view of eq. (5), the above expressions give:

\[
\sqrt{\frac{\varepsilon}{\sqrt{\text{Re}_s} C_f}} = \frac{1}{1 + \lambda_2} \left\{ (1 + \beta) f''(0, \xi) - \beta(1 - \xi) \left[ \frac{\partial f''(0, \xi)}{\partial \xi} - \frac{1}{2 \xi} f''(0, \xi) \right] \right\}
\]  

(13)

\[
\frac{1}{\sqrt{\varepsilon}} \frac{1}{\sqrt{	ext{Re}_s}} \text{Nu}_x = -\theta'(0, \xi)
\]  

(14)

where \(\text{Re}_s = \frac{u \nu}{\nu}\) is the local Reynolds number.

**Steady-state flow** (\(\xi = 1\))

This solution corresponds to \(\xi = 1\), where \(f_s(\eta, 1)\) and \(\theta(\eta, 1) = \theta_s(\eta)\). In this case eqs. (6)-(8) reduce to:

\[
f_s'' + (1 + \lambda_2)(-f_s'' + f_s f_s'') + \beta(f_s''^2 - f_s f_s') = 0,
\]  

(15)

\[
(1 + \lambda_2)(\theta_s'' + \text{Pr} f_s' \theta_s') + \text{Pr Ec}[f_s''^2 + \beta(f_s' f_s''^2 - f_s' f_s f_s'')] = 0
\]  

(16)

\[
f_s(0) = 0, \quad f_s'(0) = 1, \quad \theta_s(0) = 1, \quad f_s'('\infty') = 0, \quad \theta_s('\infty') = 0
\]  

(17)

It is important to note that exact solution of eq. (15) subject to boundary conditions (17) has the form:

\[
f_s(\eta) = \frac{1 - e^{-\eta m}}{m}; \quad m = \frac{1 + \lambda_2}{1 + \beta}
\]  

(18)

After substituting the expression of \(f_s\) from eq. (18) in eq. (16) we have solved the resulting differential equation numerically by a symbolic computation software MATHEMATICA.

**Computations by homotopy analysis method (HAM)**

**Zeroth-order deformation problems**

We select the initial guesses and the linear operator as:

\[
f_0(\eta, \xi) = 1 - e^{-\eta}, \quad \theta_0(\eta, \xi) = e^{-\eta}
\]  

(19)

\[
L_f(f) = f'' - f'
\]  

(20)

\[
L_\theta (f) = f'' - f
\]  

(21)

where \(L_f\) and \(L_\theta\) satisfy the following properties:

\[
L_f(A_1 e^\eta + A_3 e^{-\eta}) = 0
\]  

(22)

\[
L_\theta(A_4 e^\eta + A_5 e^{-\eta}) = 0
\]  

(23)
where \( A(i = 1-5) \) are the arbitrary constants and the non-linear operators \( N_f \) and \( N_q \) are:

\[
N_f[\tilde{f}(\eta, \xi; p)] = \left[ \xi - \beta(1 - \xi) \right] \frac{\partial^3 \tilde{f}(\eta, \xi; p)}{\partial \eta^3} + \\
(1 + \lambda_2) \cdot \left[ \xi \left( \left( \frac{\partial \tilde{f}(\eta, \xi; p)}{\partial \eta} \right)^2 - \tilde{f}(\eta, \xi; p) \right) \frac{\partial^2 \tilde{f}(\eta, \xi; p)}{\partial \eta^2} \right] + \\
(1 - \xi) \left( \frac{\eta \frac{\partial^4 \tilde{f}(\eta, \xi; p)}{\partial \eta^4}}{2} - \frac{\xi \frac{\partial^4 \tilde{f}(\eta, \xi; p)}{\partial \eta^4}}{2} \right) + \xi \left( \left( \frac{\partial^2 \tilde{f}(\eta, \xi; p)}{\partial \eta^2} \right)^2 - \tilde{f}(\eta, \xi; p) \right) \frac{\partial^3 \tilde{f}(\eta, \xi; p)}{\partial \eta^3}
\]

\[
N_q[\tilde{q}(\xi, \eta, p), \tilde{q}(\xi, \eta, p)] = \xi \frac{\partial^2 \tilde{q}(\xi, \eta, p)}{\partial \eta^2} + \frac{Pr \xi}{1 + \lambda_2} \left( \xi \frac{\partial^2 \tilde{q}(\xi, \eta, p)}{\partial \eta^2} \right)^2 + \\
+ \frac{Pr Ec \beta}{1 + \lambda_2} \left[ \xi \frac{\partial^2 \tilde{q}(\xi, \eta, p)}{\partial \eta^2} \right]^3 + \\
+ \frac{Pr Ec \beta}{1 + \lambda_2} \left[ \xi \frac{\partial^2 \tilde{q}(\xi, \eta, p)}{\partial \eta^2} \right]^3 
\]

The problems at the zeroth order are:

\[
(1 - p)L_f[\tilde{f}(\eta, \xi, p)] - f_0(\eta, \xi) = ph_f N_f[\tilde{f}(\eta, \xi, p)] \tag{26}
\]

\[
(1 - p)L_q[\tilde{q}(\xi, \eta, p), \tilde{q}(\xi, \eta, p)] - \theta_0(\eta, \xi) = ph_q N_q[\tilde{q}(\xi, \eta, p), \tilde{q}(\xi, \eta, p)] \tag{27}
\]

\[
\tilde{f}(0, \xi, p) = 0, \quad \tilde{f}'(0, \xi, p) = 1, \quad \tilde{q}(0, \xi, p) = 1, \quad \tilde{q}'(0, \xi, p) = 0, \quad \tilde{q}(0, \xi, p) = 0 \tag{28}
\]

In the above equations \( h_f \) and \( h_q \) are auxiliary non-zero parameters and \( p \in [0,1] \) is an embedding parameter. For \( p = 0 \) and \( p = 1 \), one has:

\[
\tilde{f}(\eta, \xi, 0) = f_0(\eta, \xi), \quad \tilde{f}(\eta, \xi, 1) = f(\eta, \xi), \tag{29}
\]

\[
\tilde{q}(\eta, \xi, 0) = \theta_0(\eta, \xi), \quad \tilde{q}(\eta, \xi, 1) = \theta(\eta, \xi) \tag{30}
\]

When \( p \) increases from 0 to 1, \( \tilde{f}(\eta, \xi, p) \) and \( \tilde{q}(\eta, \xi, p) \) vary continuously from the initial guesses \( f_0(\eta, \xi) \) and \( \theta_0(\eta, \xi) \) to the final solutions \( f(\eta, \xi) \) and \( \theta(\eta, \xi) \). By Taylor's theorem and eqs. (29) and (30) we get:

\[
\tilde{f}(\eta, \xi, p) = f_0(\eta, \xi) + \sum_{m=1}^{\infty} f_m(\eta, \xi)p^m; \quad f_m(\eta, \xi) = \frac{1}{m!} \frac{\partial^m \tilde{f}(\eta, \xi, p)}{\partial p^m} \bigg|_{p=0} \tag{31}
\]

\[
\tilde{q}(\eta, \xi, p) = \theta_0(\eta, \xi) + \sum_{m=1}^{\infty} \theta_m(\eta, \xi)p^m; \quad \theta_m(\eta, \xi) = \frac{1}{m!} \frac{\partial^m \tilde{q}(\eta, \xi, p)}{\partial p^m} \bigg|_{p=0} \tag{32}
\]
The auxiliary parameters $h_f$ and $h_q$ are so properly selected such that series solutions converge at $p = 1$. Substituting $p = 1$, one obtains:

$$f(\eta, \xi) = f_0(\eta, \xi) + \sum_{m=1}^{\infty} f_m(\eta, \xi)$$  \hspace{1cm} (33)

$$\theta(\eta, \xi) = \theta_0(\eta, \xi) + \sum_{m=1}^{\infty} \theta_m(\eta, \xi)$$  \hspace{1cm} (34)

$m^{th}$-order deformation problems

The problems at this order are:

$$L_f \left[ f_m(\eta, \xi, p) - \chi_m f_{m-1}(\eta, \xi) \right] = h_1 R_{1,m}(\eta, \xi)$$  \hspace{1cm} (35)

$$L_0 \left[ \theta_m(\eta, \xi, p) - \chi_m \theta_{m-1}(\eta, \xi) \right] = h_0 R_{2,m}(\eta, \xi)$$  \hspace{1cm} (36)

$$f_m(0, \xi) = f'_m(0, \xi) = f'_m(\infty, \xi) = \theta_m(0, \xi) = \theta_m(\infty, \xi) = 0$$  \hspace{1cm} (37)

$$R_{1,m}(\eta, \xi) = [\xi - \beta(1 - \xi)] f'_m + \left( 1 + \lambda_2 \right) (1 - \xi) \left( \frac{n}{2} \xi f''_m - \xi^2 \frac{\partial f'_m}{\partial \xi} \right) + \beta(1 - \xi) \left( \frac{n}{2} f''_m + \xi \frac{\partial f'_m}{\partial \xi} \right) + \sum_{k=0}^{\infty} \left( 1 + \lambda_2 \right) \xi^2 f_m + \beta(1 - \xi) \left( \frac{n}{2} \xi f''_m - \xi^2 \frac{\partial f'_m}{\partial \xi} \right) + \beta(1 - \xi) \left( \frac{n}{2} f''_m + \xi \frac{\partial f'_m}{\partial \xi} \right) + \sum_{k=0}^{\infty} \left( 1 + \lambda_2 \right) \xi^2 f_m$$

$$R_{2,m}(\eta, \xi) = \xi \theta''_m - \Pr \left( 1 - \xi \right) \left( \frac{n}{2} \xi \theta''_m - \xi \frac{\partial \theta'_m}{\partial \xi} \right) + \frac{\Pr \Ec}{1 + \lambda_2} \left[ \xi (1 - \xi) \sum_{k=0}^{\infty} \xi^2 \xi f_m - \xi \frac{\partial f'_m}{\partial \xi} \right]$$  \hspace{1cm} (38)

$$f_m(\eta, \xi) = f'_m(\eta, \xi) + A_1 + A_2 e^\eta + A_3 e^{-\eta}$$  \hspace{1cm} (41)

$$\theta_m(\eta, \xi) = \theta''_m(\eta, \xi) + A_4 e^\eta + A_5 e^{-\eta}$$  \hspace{1cm} (42)

where $f'_m(\eta, \xi)$ and $\theta''_m(\eta, \xi)$ denote the special solutions in eqs. (41) and (42) and $A_i (i = 1-5)$ can be determined by using the boundary conditions (37). These are:

$$A_2 = A_4 = 0, \quad A_3 = -\frac{\partial f'_m(\eta, \xi)}{\partial \eta} \bigg|_{\eta=0}, \quad A_1 = -A_3 - f'_m(0, \xi), \quad A_5 = -\theta''_m(0, \xi)$$  \hspace{1cm} (43)

Note that the problems consisting of eqs. (35)-(43) can be solved by employing the symbolic computation software MATHEMATICA for $m = 1, 2, 3, \ldots$
Analysis of convergence

We notice that eqs. (33) and (34) contain the auxiliary parameters \( h_f \) and \( h_0 \). These parameters can be used to adjust the convergence rate of the derived series solutions. To obtain the proper values of these parameters which give the convergent series solutions, the so called \( h_f \) and \( h_0 \)-curves have been plotted in figs. 1 and 2 for some fixed values of parameters. The interval on \( h \)-axis for which the \( h_f \) and \( h_0 \)-curves becomes parallel to the \( h \)-axis is considered to be the set of admissible values of \( h_f \) and \( h_0 \). It is found that when \( \xi = 0.5 \) the permissible values of \( h_f \) and \( h_0 \) are \(-1.1 \leq h_f \leq -0.5 \) and \(-1.7 \leq h_0 \leq -0.7 \), respectively. The \( h_f \)-curves for different values of \( \xi \) have also been sketched. It is observed that valid range for the \( h_f \) slightly shrinks with an increase in \( \xi \). The obtained results indicate that the series solutions converge for all dimensionless time \( \tau(0 \leq \tau < \infty) \) in the whole spatial domain \( (0 \leq \eta < \infty) \).

Results and discussion

This section emphasizes the significance of emerging parameters on the velocity, temperature, coefficient of skin friction and local Nusselt number. It is found that when \( h = -0.5 \) and \( \xi = 1.0 \), the 5th-order homotopy solution agrees well with the exact solution, eq. (17). Furthermore, increase in the values of Deborah number \( \beta \) corresponds to an increase in the velocity and the boundary layer thickness. However opposite trend is noticed for the parameter \( l_2 \). Temperature \( \theta_1 (\eta) \) has been plotted vs. \( \eta \) for different values of Pr and Ec. It is clear from these figs. 3 and 4 that analytic solutions obtained by HAM are in a very good agreement with the numerical solutions computed by MATHEMATICA. Figure 5 shows the behavior of dimensionless time \( \tau \).
on the velocity and the boundary layer thickness. It is seen that the velocity profiles develop rapidly from rest as \( t \) increases until the steady-state situation (\( t \rightarrow \infty \)) is achieved. Figure 6 explores the behavior of \( \beta \) on the velocity field \( f' \). Small Deborah numbers \( \beta \leq 1 \) characterize the liquid-like behavior. However, the solid-like behavior is associated with large Deborah numbers. Keeping this fact in mind we have only displayed the graphs for small values of Deborah number. It is observed that velocity field \( f' \) is an increasing function of \( \beta \). Figure 7 examines the influence of dimensionless time \( \tau \) on the temperature \( \theta \). An increase in \( \tau \) corresponds to an increase in the temperature and the thermal boundary layer thickness. It is worth pointing here that temperature profiles show less deviation for large values of the time. An increase in the Prandtl number \( \text{Pr} \) corresponds to a decrease in the temperature and the thermal boundary layer thickness. This is because for small values of the Prandtl number \( \text{Pr} \leq 1 \), the fluid is highly conductive. Physically, if \( \text{Pr} \) increases, the thermal diffusivity decreases and this phenomenon leads to the decreasing of energy transfer ability that reduces the thermal boundary
layer. It is evident from fig. 9 that the outcome of an increase in \( \beta \) is the decay of thermal boundary layer thickness. The large values of \( Ec \) give rise to a strong viscous dissipation effect which enhances the temperature and thermal boundary layer thickness (see fig. 10).

**Final remarks**

The analytic solutions for momentum and heat transfer of Jeffrey fluid have been obtained. The major points can be summarized as follows.

- An increase in elastic parameter of Jeffrey fluid (the Deborah number \( \beta \)) corresponds to an increase in the velocity and the boundary layer thickness.
- The velocity increases and the temperature rises by increasing the dimensionless time (\( \tau \)).
- The temperature and the thermal boundary layer thickness are increasing functions of Eckert number (\( Ec \)).
- Homotopy solutions are found to be in excellent agreement with the exact and numerical solutions for steady state case.

**References**


